

Electrodynamic loudspeakers

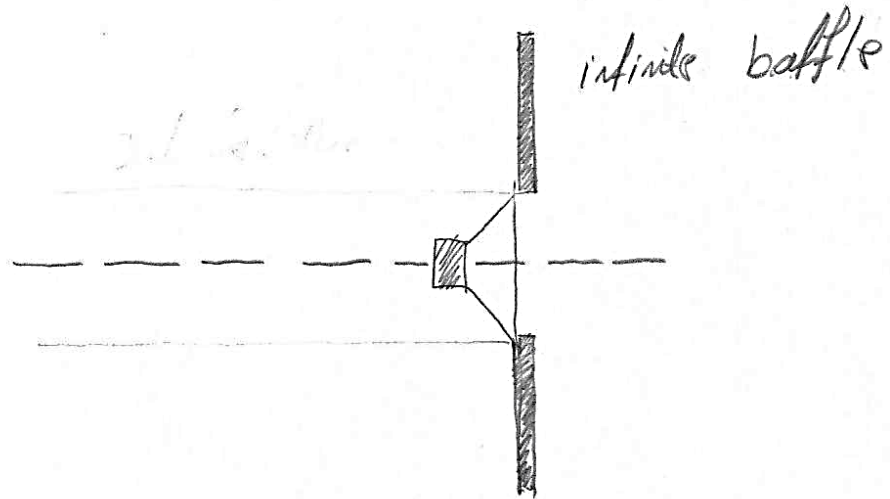
Exercise session

Pouyan Ebrahimbabaie

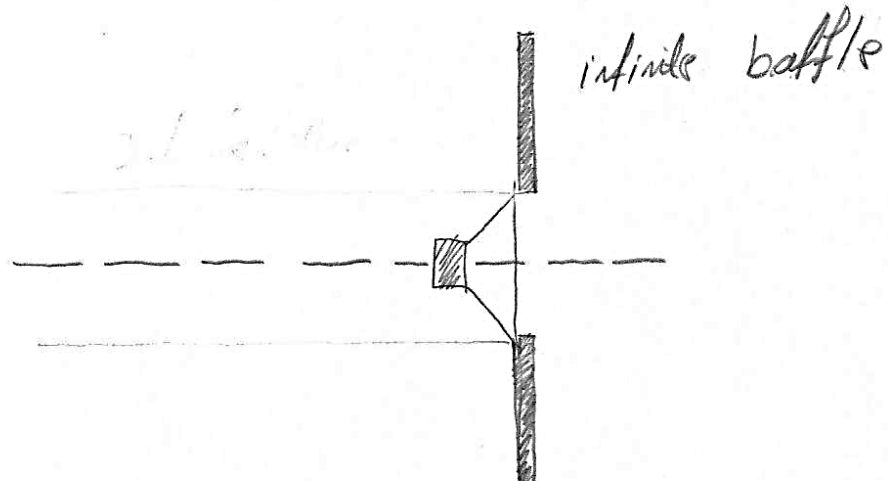
**Laboratory for Signal and Image Exploitation (INTELSIG)
Dept. of Electrical Engineering and Computer Science
University of Liège
Liège, Belgium**

**Acoustics and electroacoustics
23 April 2018**

Question 1, « problème 3 » :



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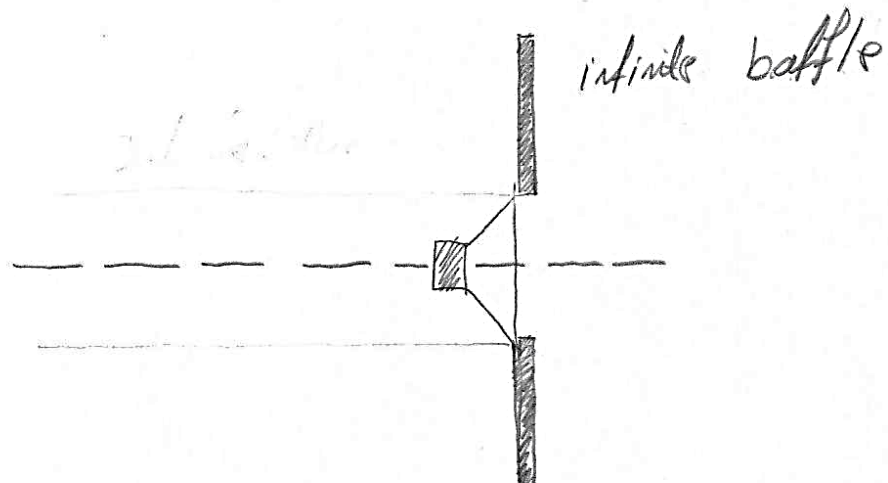


1.1)

$$f_0 = \frac{1}{2\pi \sqrt{(m_M + \frac{16}{3}\rho a^3) C_M}}$$

if $\frac{a}{\lambda} \ll 1$
at f_0

Question 1, (problème 3):



1.1)

$$f_0 = \frac{1}{2\pi \sqrt{(m_M + \frac{16}{3}\rho_0 a^3) C_M}} \quad \text{if } k \cdot \text{radius} < 0.3$$

at f_0

⚠ a is radius \equiv half of the diameter (i.e. $a = 0.1$)

⚠ if $k \cdot \text{radius} < 0.3$ at f_0

$$\Rightarrow f_0 = \frac{1}{2\pi \sqrt{0.075 + \frac{16}{3} (1.2) 10^{-3}}} = 109 \text{ Hz}$$

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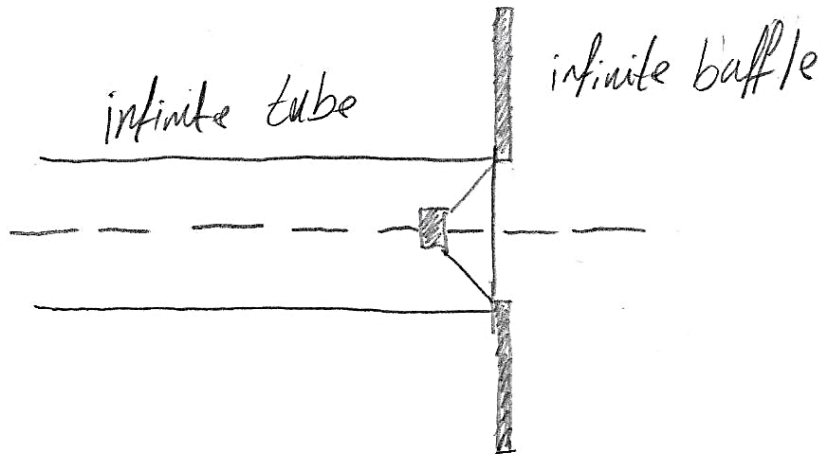
$$\text{Check: @ } f_0 = 109 \text{ Hz, } ka = \frac{2\pi f a}{c} = 0.20 < 0.3$$

ok

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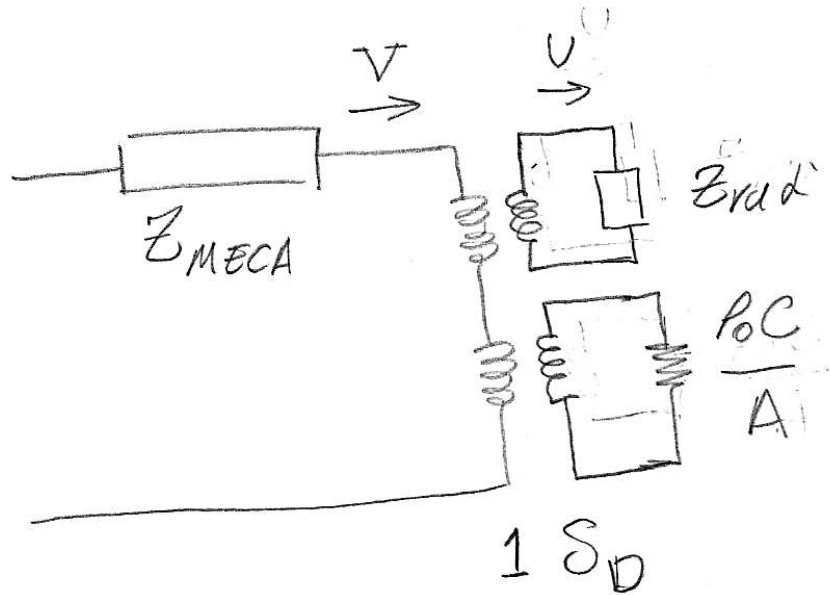
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1.2)



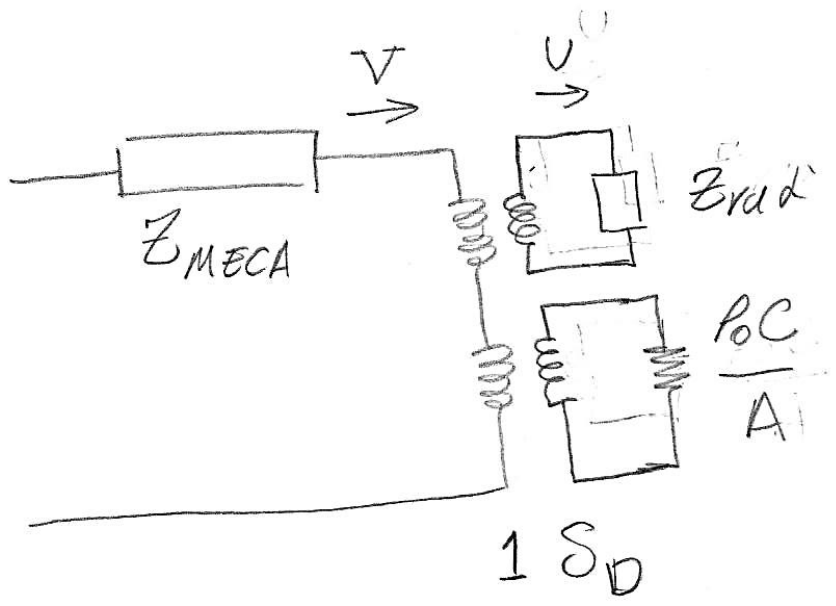
Electroacoustic model

Electroacoustic model



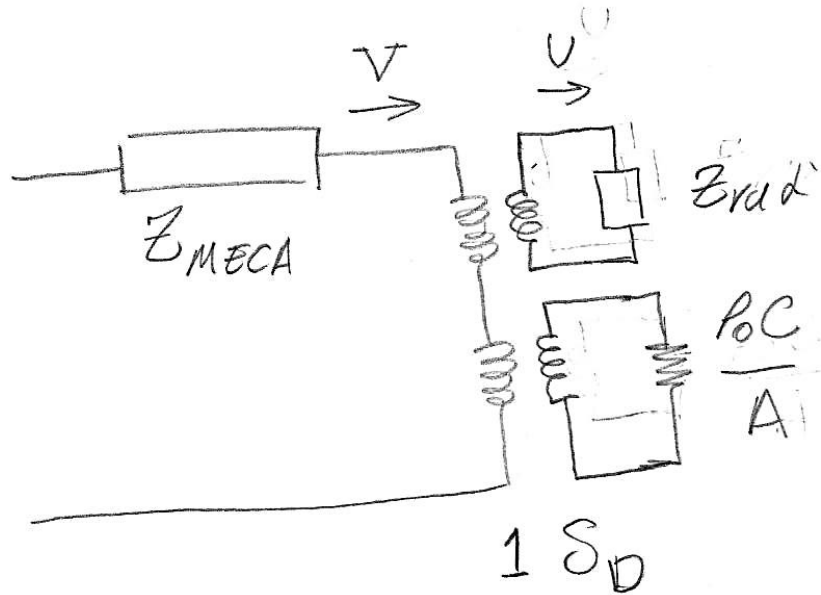
S_D : is surface of the membrane

Electroacoustic model



S_D : is surface of the membrane

Electroacoustic model



(radiation impedance
in infinite baffle)

A : is the
cross section of
the infinite tube

S_D : is surface of the membrane

With infinite tube, the resonance freq

is:

$$f_0 = \frac{1}{2\pi \sqrt{(m_M + \frac{8}{3} \rho_0 a^3) C_M}}$$

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unchanged

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unchanged

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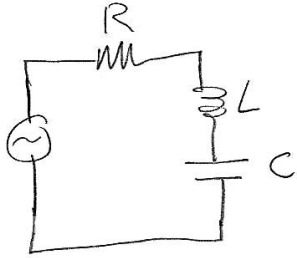
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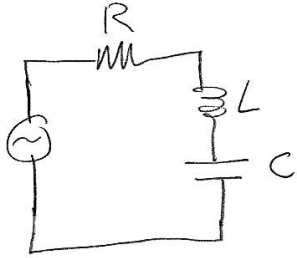
Explanation:

resonance frequency of RLC circuit



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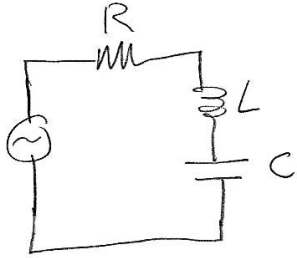
resonance frequency of RLC circuit



$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

Explanation:

resonance frequency of RLC circuit

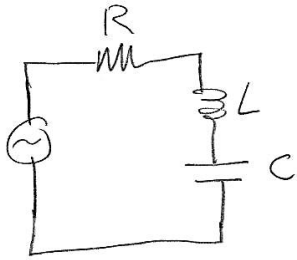


$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

depends only on inductance
and capacitance.

Explanation:

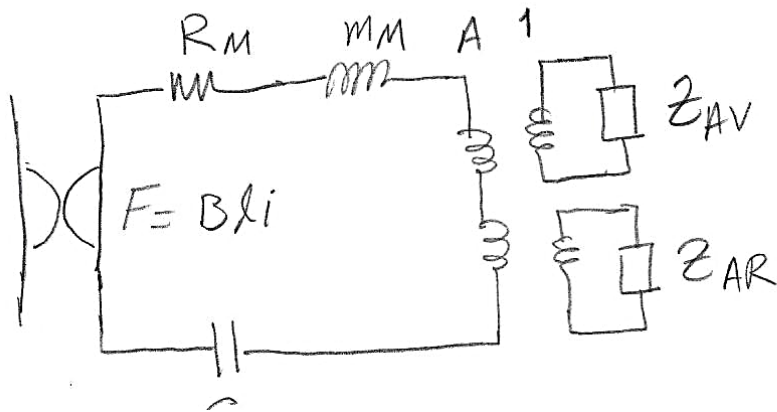
resonance frequency of RLC circuit



$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

depends only on inductance and capacitance.

infinite baffle without tube:



$$A^2 Z_{AV} = A^2 Z_{AR}$$

$$= \text{circle} + j\omega \frac{8\rho a^3}{3}$$

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(Avant)

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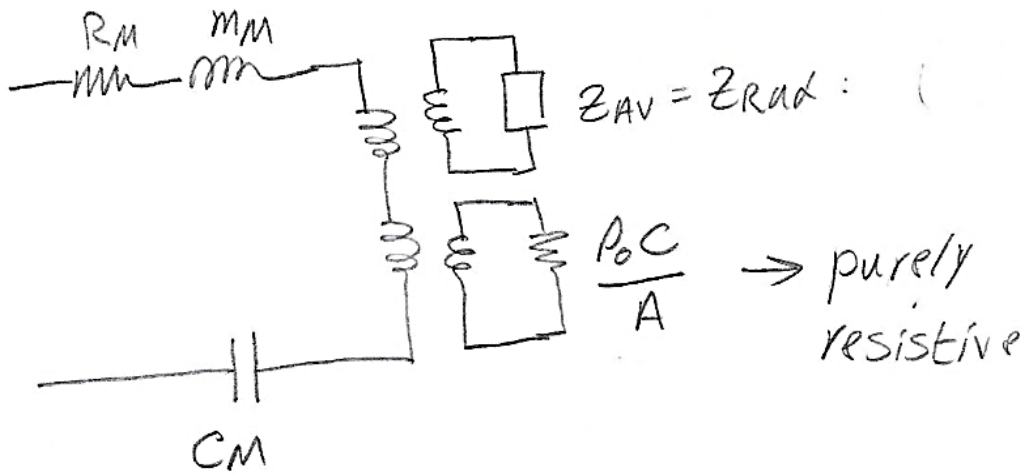
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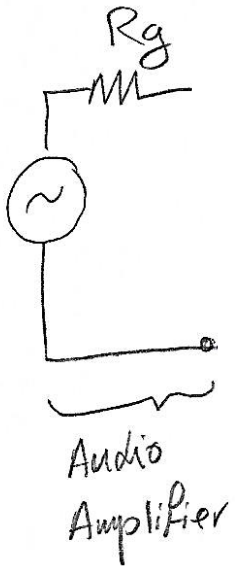
infinite tube and infinite battery:



$$f_0' = \frac{1}{2\pi \sqrt{(m_M + \frac{8\rho a^3}{3}) C_M}}$$

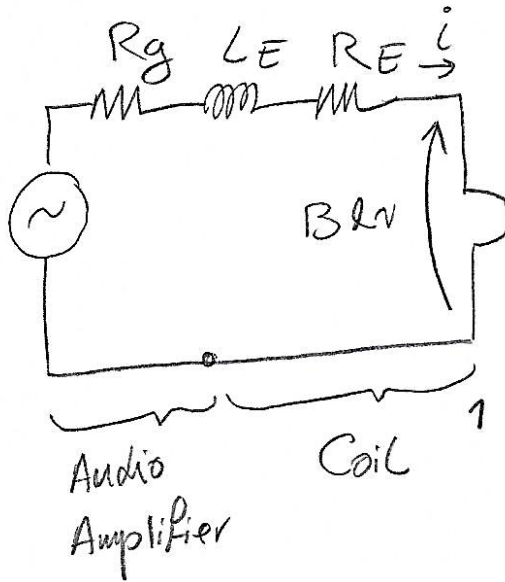
1.3)

electroacoustic model at 1 kHz



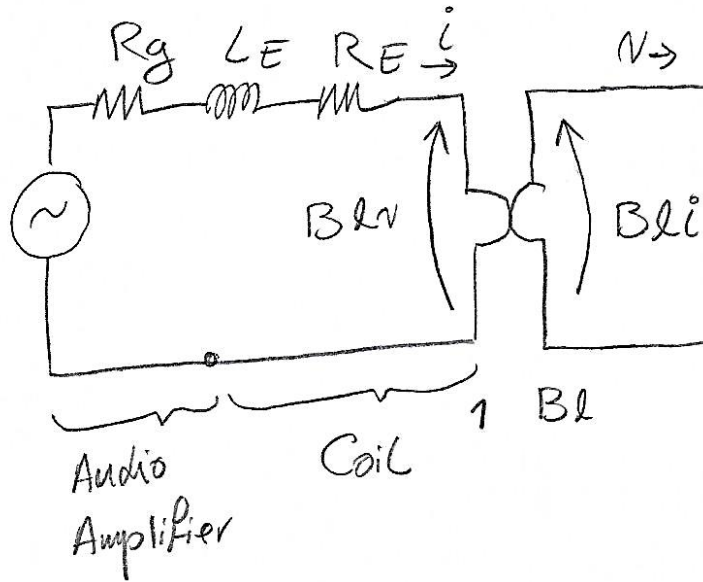
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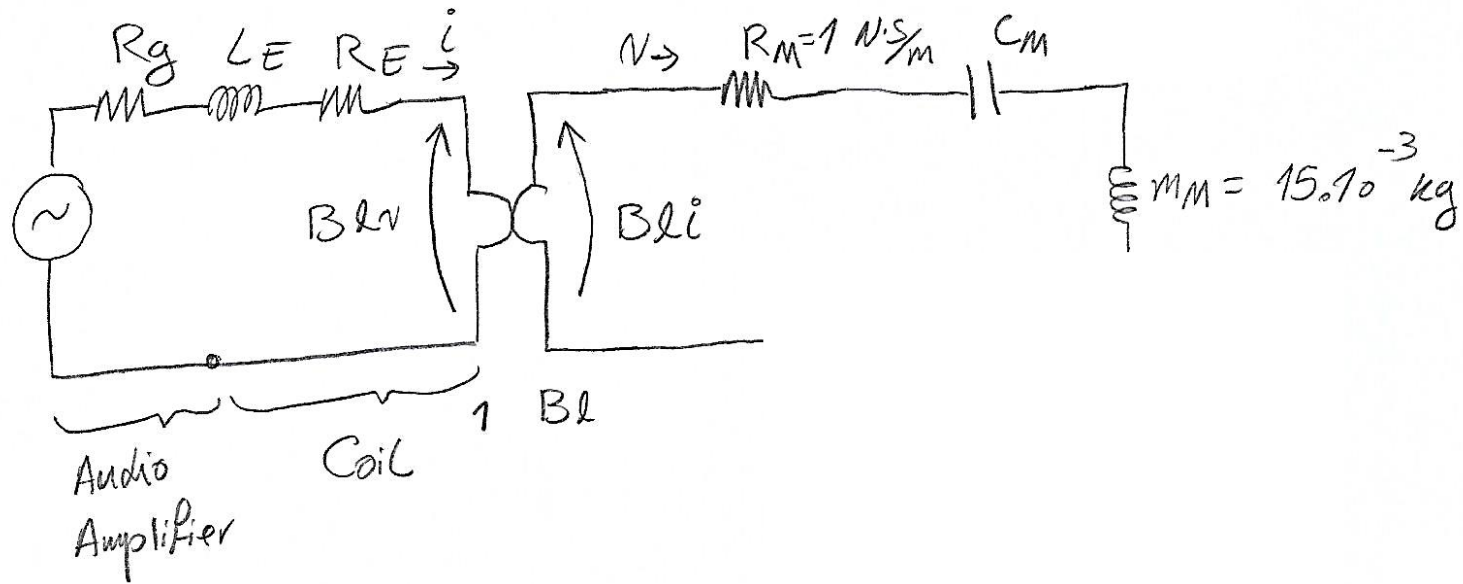
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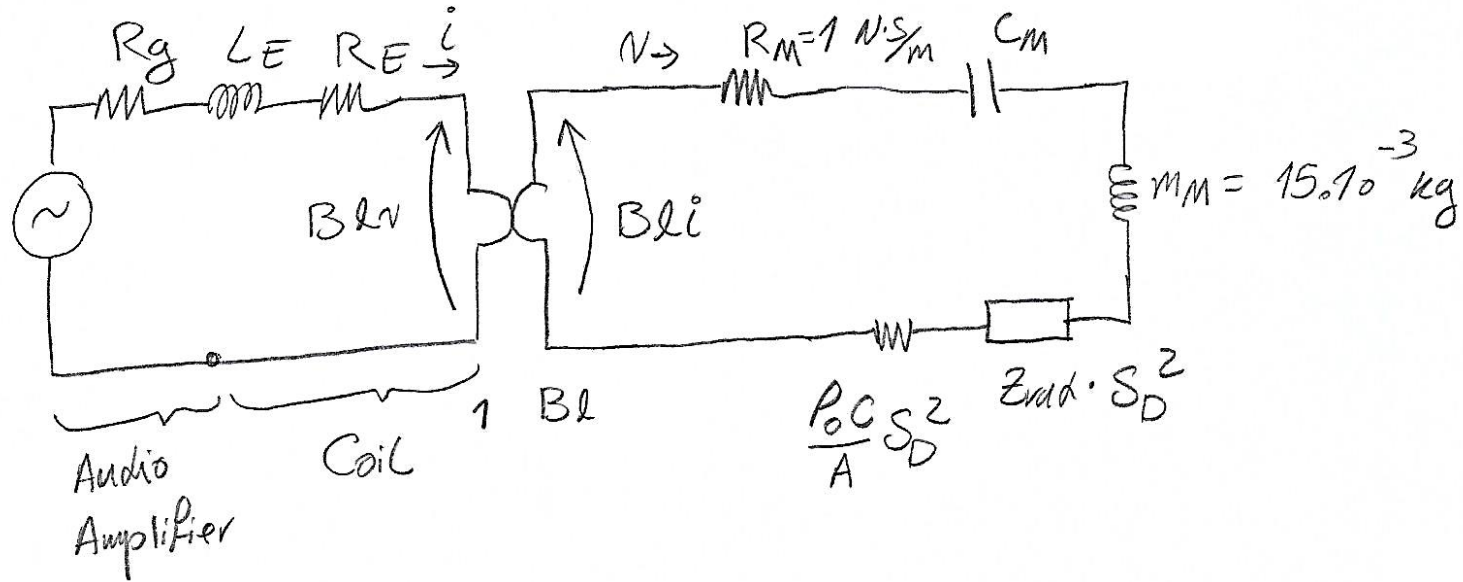
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" 10⁻²

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$$\Rightarrow R_{MR} = \text{real}\left\{\frac{\rho_0 c}{\pi a^2} \cdot (\pi a^2)^2 (1 + j0.6)\right\} = 12.8 \text{ N}\cdot\text{s}/\text{m}$$

$$\rightarrow \text{with } Z_{MT} = R_M + j\omega m_M + \frac{1}{j\omega C_M} + \delta_D^2 \left(\frac{\rho_0 c}{A} + Z_{rad}\right)$$

↳ total mechanic impedance, including acoustic one

$$\Rightarrow Z_{MT} = 1 + j94.25 + 0 + P_0 C(\pi a^2) (1 + 1 + j0.6)$$

$$\Rightarrow Z_{MT} = 1 + j94.25 + \underbrace{0 + P_0 C (\pi a^2) (1 + 1 + j0.6)}_{25.6 + j(7.7)}$$

approx.

(Can be neglected)

if $f = 1 \text{ kHz} \gg f_0$

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most of the time $\eta < 10\%$

1.5)

$$\left| \frac{P_{rms @ 1m}}{e_{g,rms}} \right| = \frac{P_0 \omega}{2\pi} S_D \frac{(Bl)/R_E}{\left| \frac{(Bl)^2}{R_E} + Z_{MT} \right|}$$

if $R_g \approx 0 \Omega$

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if $R_g \approx 0 \Omega$

$$= (1.2)(1000)(\pi a^2) \frac{(10.52/10)}{|11.07 + 26.6 + j103|}$$

$$\approx 0.35 \text{ Pa}/\sqrt{\text{V}}$$

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if $e_{g,rms} = 1V \Rightarrow P_{rms} @ 1m = 0.35 \text{ Pa}$

$$\Rightarrow P_{rms} @ 4m = \frac{0.35}{4} (\sim 73 \text{ dB})$$

↓
~ Spherical wave

1.6) Maximum displacement @ 1 kHz

Input electric power = 10 W

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= 15 μm (rms)

Question 2/ (Exercise 2):

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Missing Elements:

$$C_M = ?$$

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\downarrow \downarrow
0.09 0.0216

in an infinite Baffle

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$$\Rightarrow C_M = (7772)^{-1} \text{ m/N}$$

$$Q_{MS} = 9.8 = \frac{1}{R_{Mt}} \sqrt{\frac{m_M + \frac{1}{3}\rho_0 a^3}{C_M}} \Rightarrow$$

$$R_{MT} = R_M + Z \left(\frac{\rho_0 \pi}{2c} a^4 \omega^2 \right) \Rightarrow \boxed{R_M \approx 2.6 \frac{N \cdot s}{m}}$$

Other parameters of electroacoustic model are known:

$$2.2) \quad P_{rms} \Big|_{@1m} = \frac{\rho_0 \omega a^2}{2} \frac{(Bl) (I_{g,rms})}{R_E \left[\frac{(Bl)^2}{R_E} + Z_{MT} \right]} \quad \overbrace{\hspace{10em}} = 1W$$

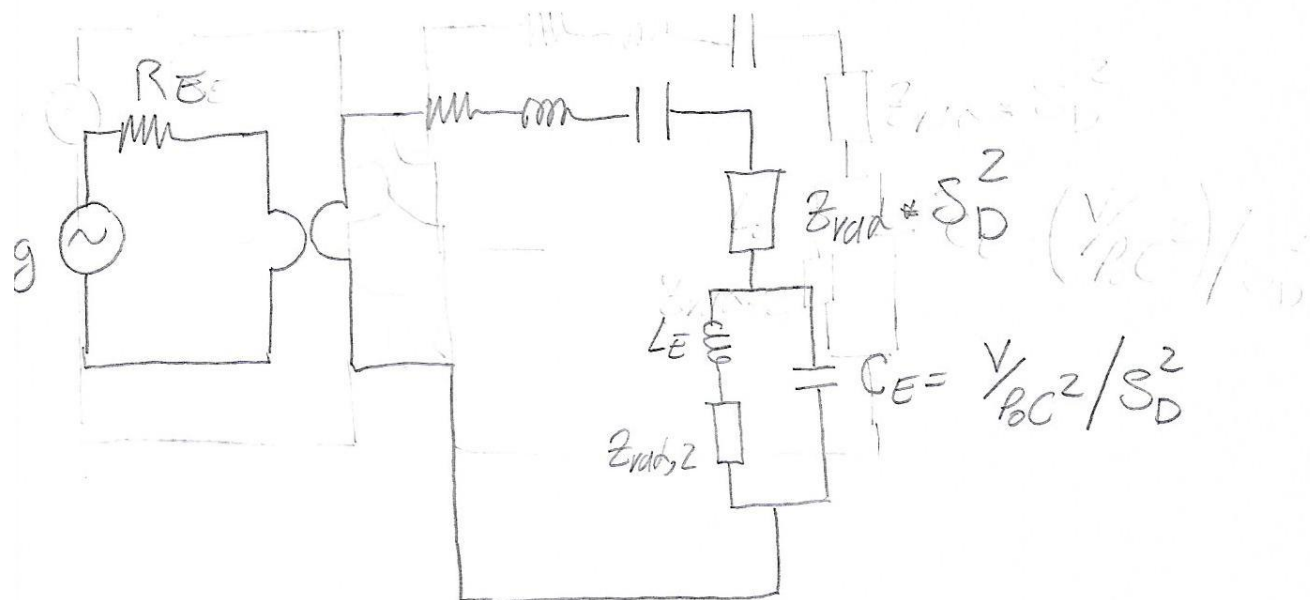
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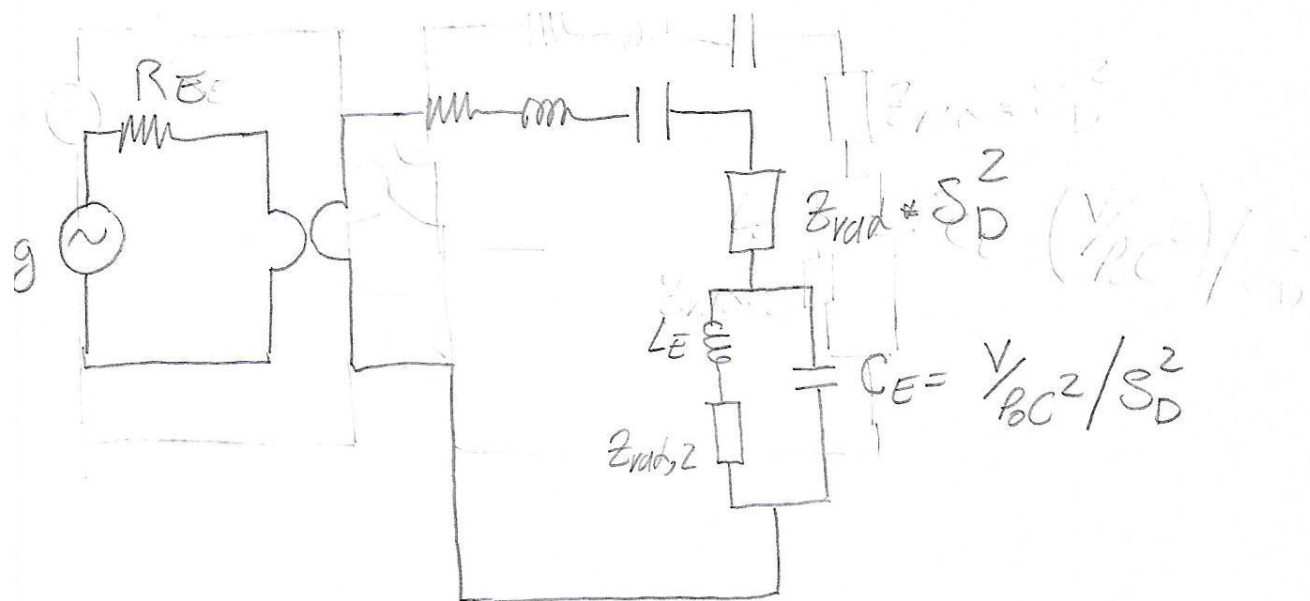
$$2.2) \quad P_{rms} \Big|_{@1m} = \frac{\rho_0 \omega a^2}{Z} \overbrace{(Bl) (I_{g,rms})}^{= 1V} \frac{1}{R_E \left[\frac{(Bl)^2}{R_E} + Z_{MT} \right]}$$

$$= 0.139 \quad (\text{or } 76.9 \text{ dB})$$

2.3)



2.3)



$V =$ volume of the box

$Z_E = \left(\frac{\rho_0 l_E}{S_E} \right) S_D^2$ acoustic impedance of the tunnel (vent)
 Length: l_E
 Cross-section: S_E

$Z_{\text{rad}, 2}$: radiation impedance of the vent
(multiplied by δ_D^2 in the mechanical part)

$$\hookrightarrow \text{imaginary part} = \omega \left(\frac{8\rho_0}{3\pi^2} \right) \frac{1}{aE} * \delta_D^2$$

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a_E = radius of the vent section



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$$35 = \frac{1}{2\pi \sqrt{\frac{V}{\rho_0 C^2} \left(\frac{\rho_0 L_E}{S_E} + \frac{8}{3} \frac{\rho_0}{\pi^2 a_E} \right)}}$$

2.4) Resonance @ 35 Hz for the tunnel.

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Several selection:

eg. if $a_E = 5 \text{ cm}$

$$\begin{aligned} \Rightarrow S_E &= \pi \cdot 25 \text{ cm}^2 \\ &= 0.785 \cdot 10^{-2} \text{ m}^2 \end{aligned}$$

$$\Rightarrow l_E = 15 \text{ cm}$$