

# **Sabine theorem**

## **Exercise session**

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**Acoustics and Electroacoustics  
5 November 2019**

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length 50 m

width 20 m

height 8 m

$V = \text{room volume} = 50 \times 20 \times 8 = 8000 \text{ m}^3$

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$\delta_{\text{abs}}$  : unknown

$$a \geq \frac{0.163 \text{ V}}{RT_{\max}}$$

$$\alpha_c \delta_c + \alpha_f \delta_f + \alpha_w \delta_w + S_{\text{abs}} (\alpha_{\text{abs}} - \alpha_w) \geq \frac{0.163 \text{ V}}{RT_{\max}}$$

$$a \geq \frac{0.163 \text{ V}}{RT_{\max}}$$

$$\underbrace{\alpha_c \delta_c + \alpha_f \delta_f + \alpha_w \delta_w}_{a'} + \underbrace{S_{\text{abs}} (\alpha_{\text{abs}} - \alpha_w)}_{> 0 \quad \forall \text{freq}} \geq \frac{0.163 \text{ V}}{RT_{\max}}$$

$$a \geq \frac{0.163V}{RT_{max}}$$

$$\underbrace{\alpha_c \delta_c + \alpha_f \delta_f + \alpha_w \delta_w}_{a'} + S_{abs} \underbrace{(\alpha_{abs} - \alpha_w)}_{> 0 \forall f_{req}} \geq \frac{0.163V}{RT_{max}}$$

$$\Rightarrow S_{abs} \geq \left( \frac{0.163V}{RT_{max}} - a' \right) / (\alpha_{abs} - \alpha_w)$$

minimum surface of  
absorbing material.

@ 250 Hz :  $S_{abs} \geq 150 \text{ m}^2$

1 kHz :  $S_{abs} \geq 360 \text{ m}^2$

4 kHz :  $S_{abs} \geq 878 \text{ m}^2$

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this one is the solution  
that is valid for other  
frequencies.



1b)  $L_p$  as a function of the distance

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Source power  
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$r$ : distance from source

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→ directivity coefficient

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$\delta_T$  = total surface of  
walls + ceiling + floor  
= 3120 m<sup>2</sup>

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$$R' = \frac{a}{1 - \alpha / \delta_T}$$

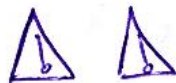
with

$$a = \sum \alpha_i \delta_i$$

$\delta_T$  = total surface of  
walls + ceiling + floor  
= 3120 m<sup>2</sup>

$$a = 1563 \text{ m}^2 \text{ @ } 1 \text{ kHz}$$

(with  $\delta_{\text{abs}} = 878 \text{ m}^2$ )



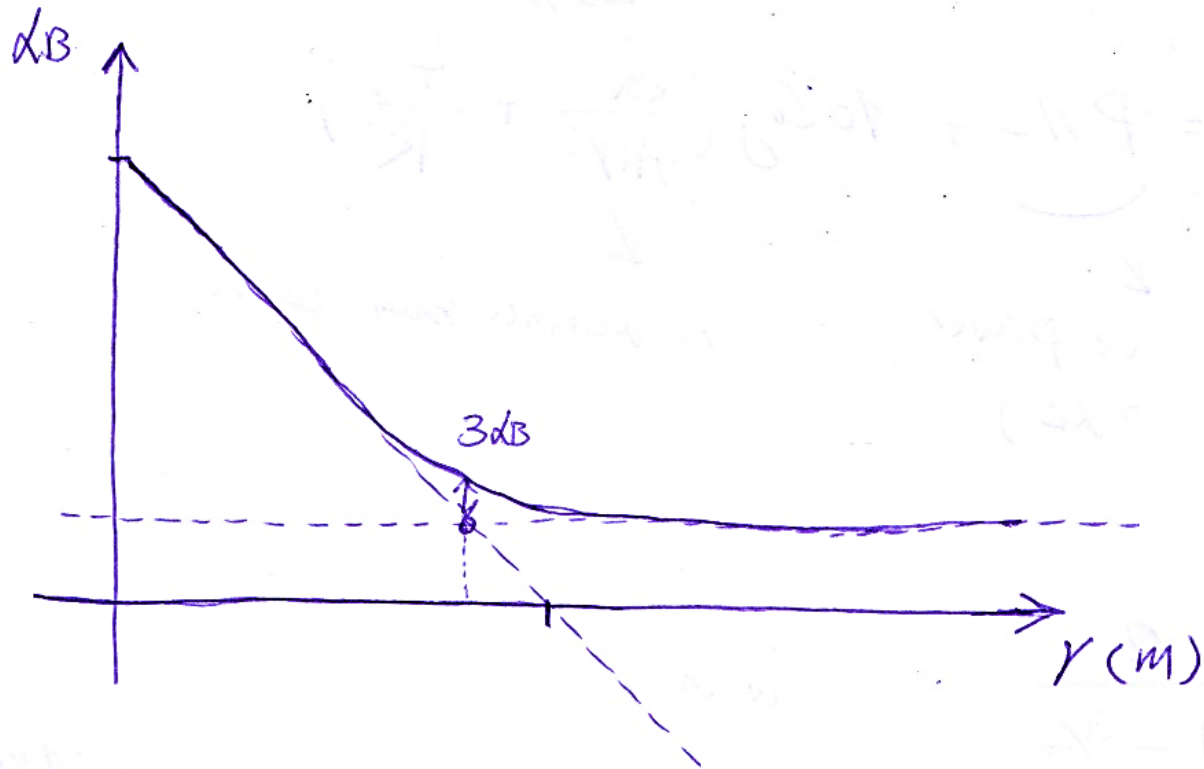


$$R' = 3133 \text{ m}^2 @ 1 \text{ kHz}$$

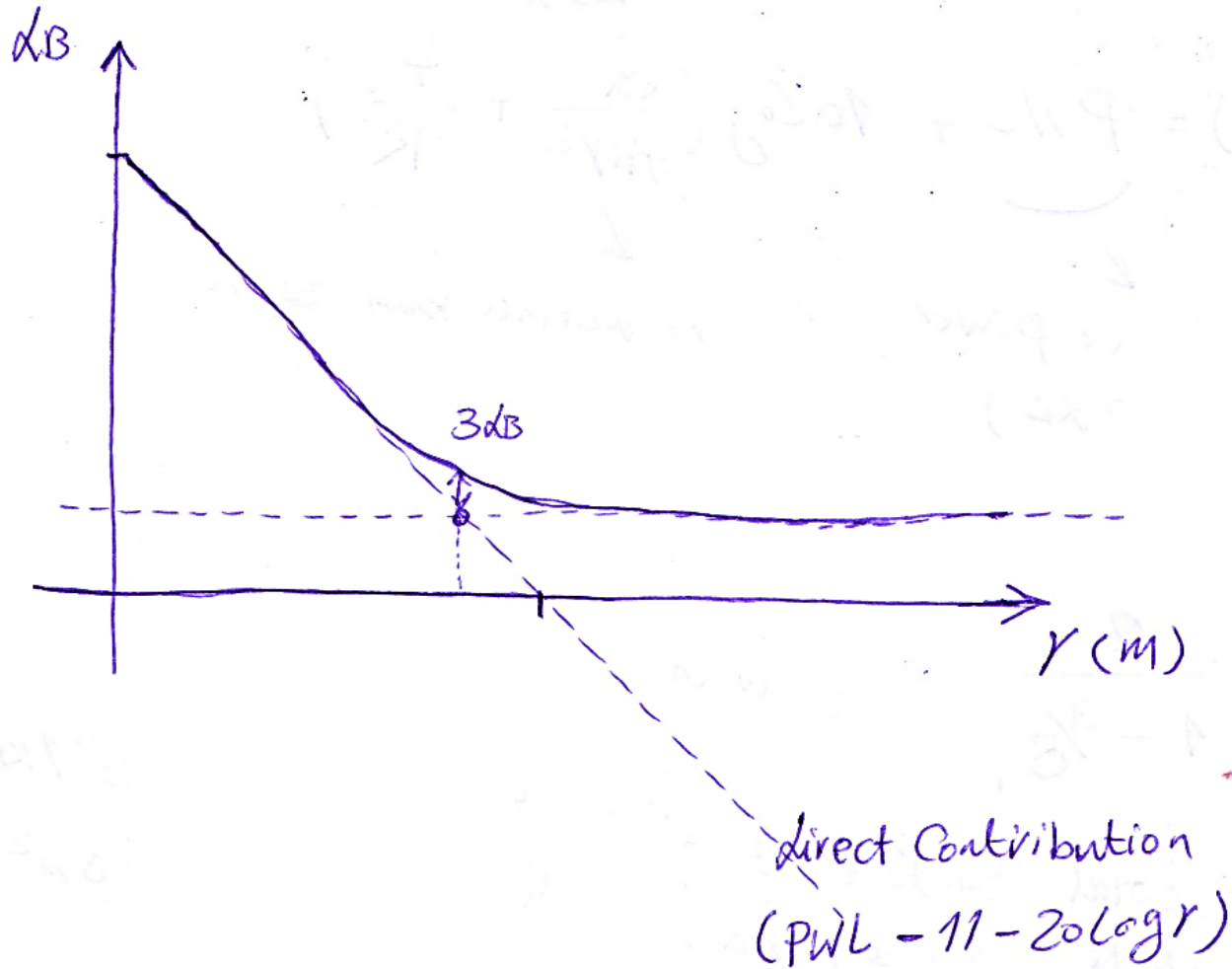
$$\Rightarrow 10 \log \frac{4}{R'} = -29 \text{ dB}$$

$$L_p(\omega) = \text{PWL} + 10 \log \left( \frac{Q}{4\pi r^2} + \frac{4}{R'} \right)$$

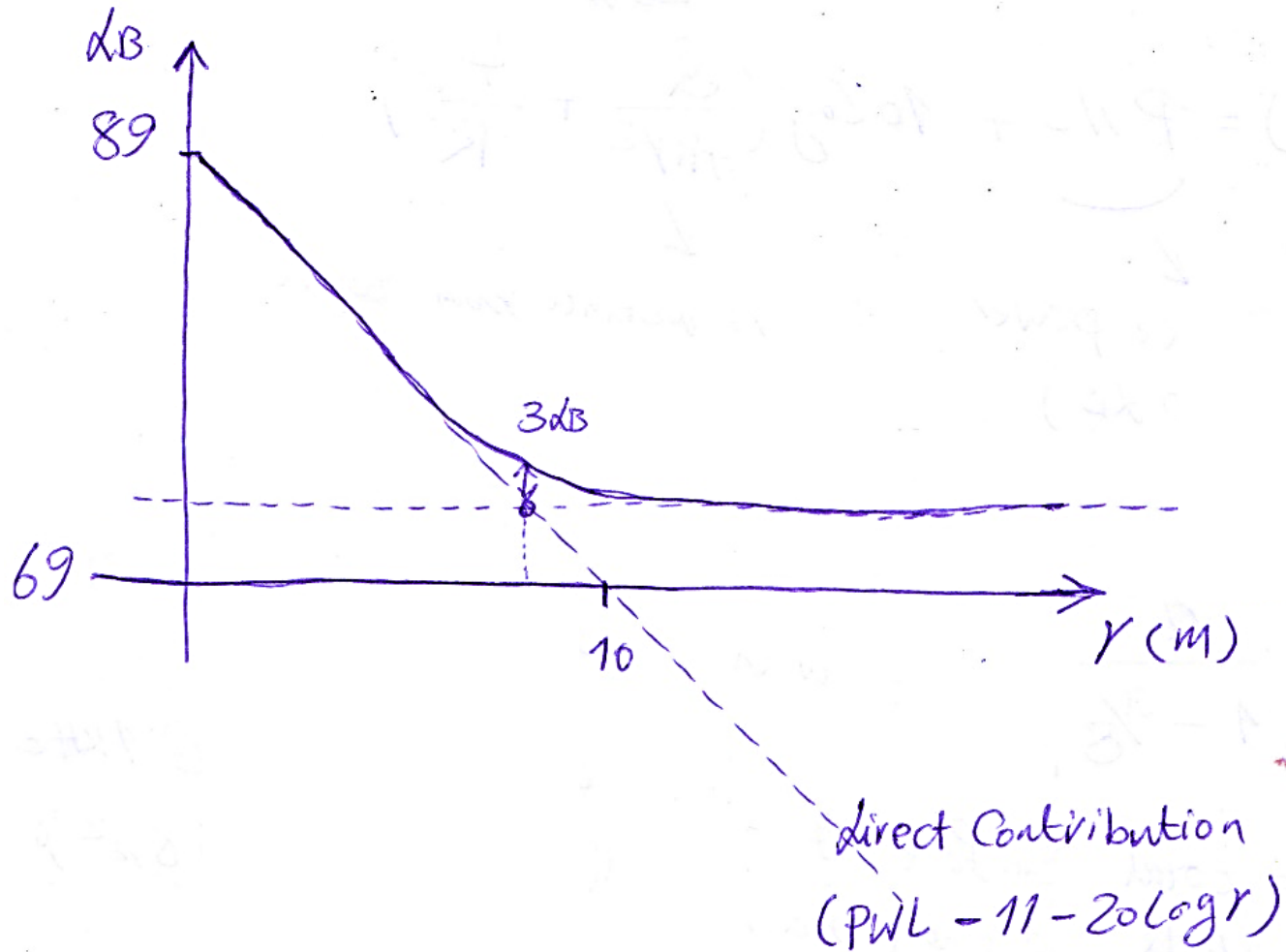
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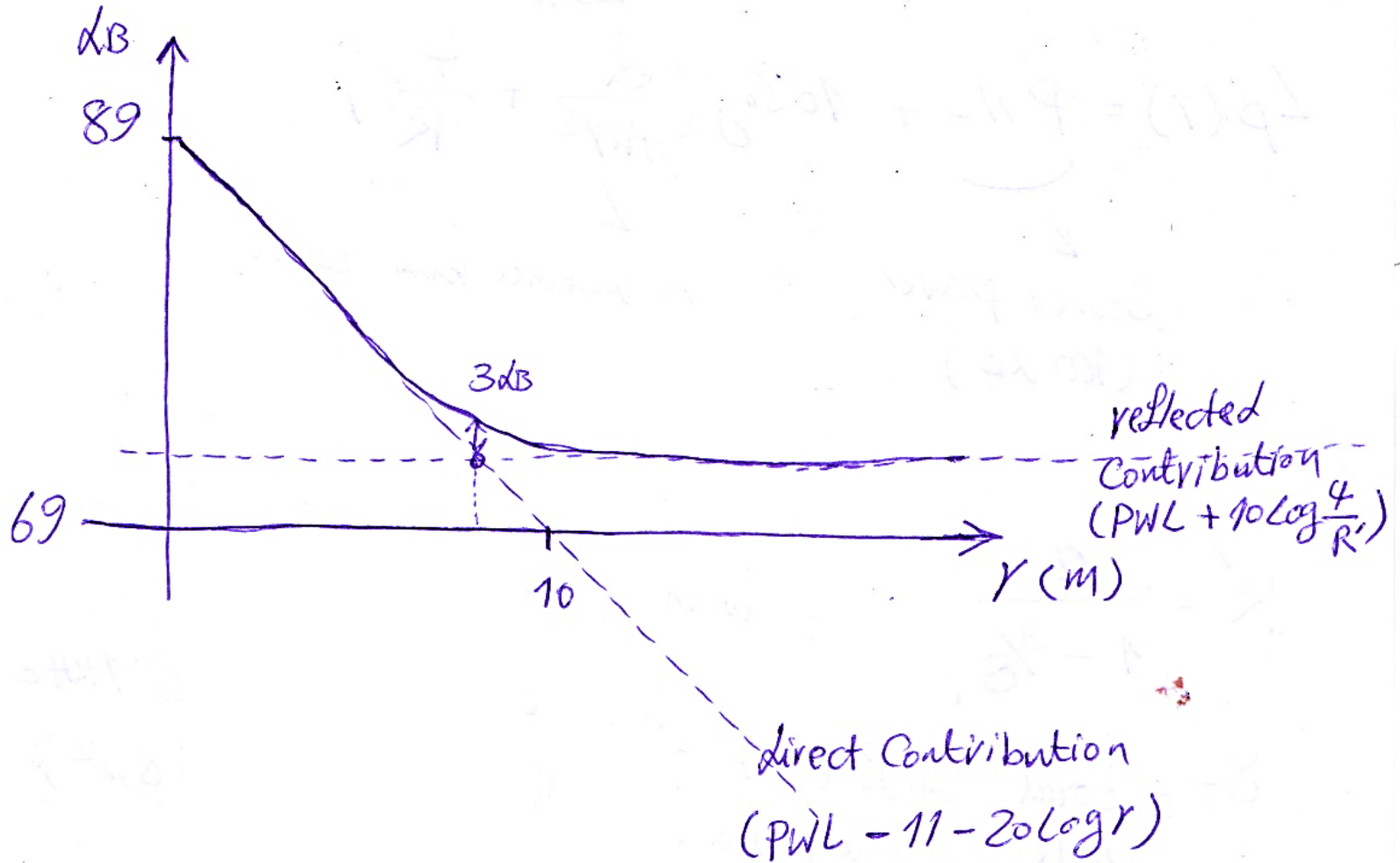
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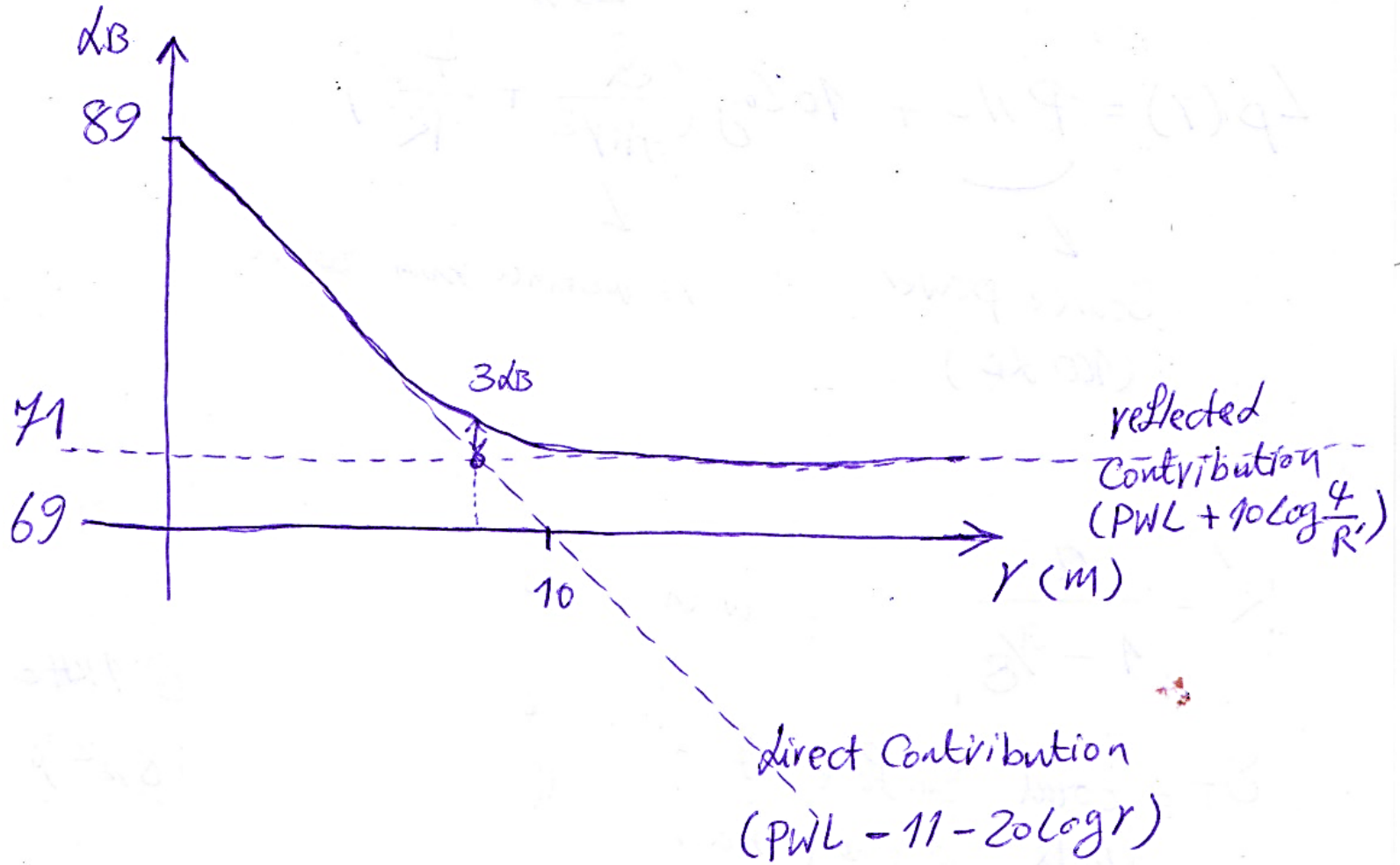
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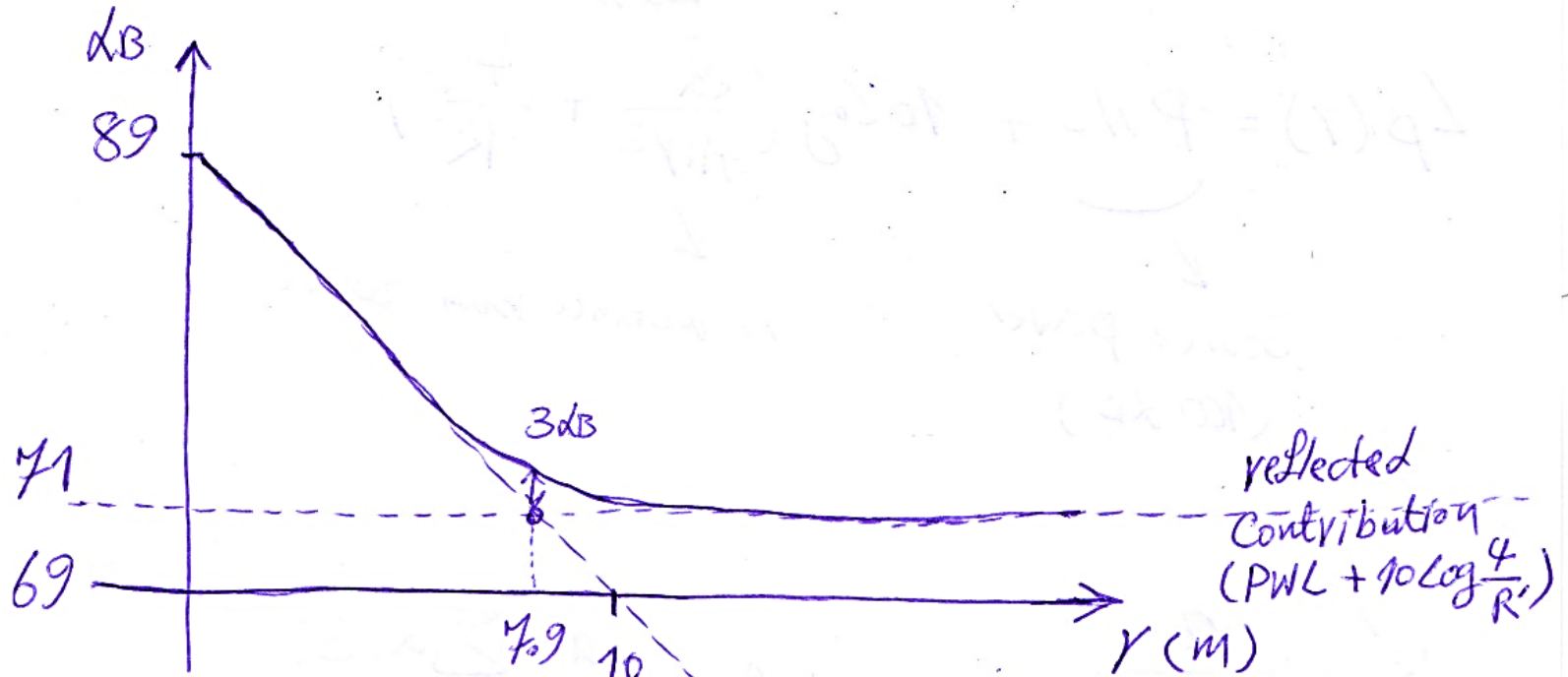
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$$\frac{1}{4} \sqrt{\frac{R'}{\pi}}$$

Reverberation  
Radius.

direct Contribution  
( $\text{PWL} - 11 - 20 \log r$ )



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$$r_{rev} = \frac{1}{4} \sqrt{\frac{R'}{\pi}}$$

$$R' = \frac{a}{1 - \alpha / \delta_T}$$

$$a = \sum \alpha_i \delta_i \quad \text{depends on Freq.}$$

$$\delta_T = \text{total surface in the room (m}^2\text{)}.$$

Data :

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method:  $RT \Rightarrow a \Rightarrow R' \Rightarrow Y_{rev}$

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$f$ (Hz)	125	250	500	1k	2k	4k
RT (s)	1.5	1.4	1.2	1.0	0.9	0.6

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$V_{rev}$ (m)	1.6	1.7	1.8	2	2.2	3.0

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→ This is the maximum distance to be in direct field at all  $f$  req.

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PWL (dB)	80	80	75	70	70	60

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R' (m <sup>2</sup> )	129	140	169	212	244	444
Lp (dB)	64.9	64.6	58.8	52.7	52.1	39.5
Correction Filter A	-16	-8	-3	0	1	1
Lp (dBA)	48.9	56.6	55.8	52.7	58.1	40.5



$L_p(\text{dBA})$  | 48.9 56.6 55.8 52.7 58.1 40.5

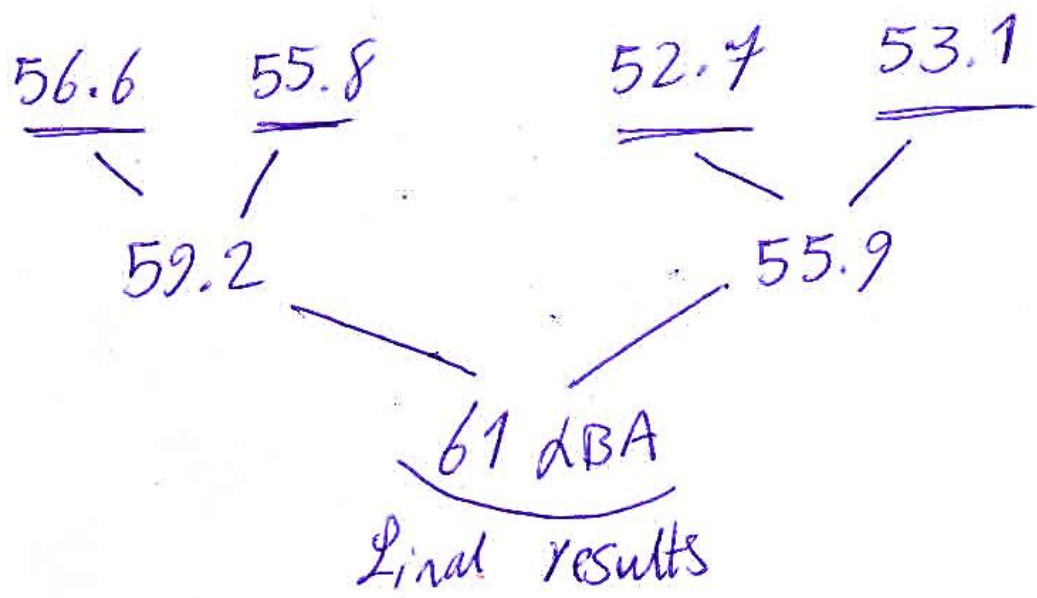
Addition in dB

$\frac{56.6}{\quad}$      $\frac{55.8}{\quad}$   
  \        /  
   59.2

$\frac{52.7}{\quad}$      $\frac{53.1}{\quad}$   
  \        /  
   55.9

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Addition in dB



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in dB      Source  
power

$$[2] \quad R' = \frac{a}{1 - a/S_T} ; \quad S_T: \text{total surface of the envelop}$$

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in dB

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Objective

$$L_{p, \text{new}} = L_{p, \text{old}} - 3 \text{dB}$$



$$[1] \Rightarrow P_{WL} + 10 \log \frac{4}{R_{\text{new}}} = P_{WL} + 10 \log \frac{4}{R_{\text{old}}} - 3 \text{dB}$$

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$$\Rightarrow 10 \log \frac{R'_{\text{old}}}{R'_{\text{new}}} = -3 \text{dB}$$

$$[1] \Rightarrow PWL + 10 \log \frac{4}{R'_{new}} = PWL + 10 \log \frac{4}{R'_{old}} - 3dB$$

$$\Rightarrow 10 \log \frac{4}{R'_{new}} = 10 \log \frac{4}{R'_{old}} - 3dB$$

$$\Rightarrow 10 \log \frac{R'_{old}}{R'_{new}} = -3dB$$

$$\Rightarrow \boxed{R'_{new} = 2 R'_{old}}$$

$$a_{old} = \underbrace{\alpha_f \delta_f}_{\text{floor}} + \underbrace{\alpha_c \delta_c}_{\text{ceiling}} + \underbrace{\alpha_w \delta_w}_{\text{bare walls}}$$

$$= (0.2)(400) + (0.2)(400) + 0.2(320) = 224 \text{ m}^2$$

$$\{2\} \Rightarrow R'_{old} = \frac{224}{1 - \frac{224}{1120}} = 80 \text{ m}^2$$

$$\{3\} \Rightarrow R'_{new} = 560 \text{ m}^2$$

$$R'_{new} = 560 \text{ m}^2 = \frac{a_{new}}{1 - \frac{a_{new}}{8T}}$$

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$$\Rightarrow a_{new} = \frac{R'_{new}}{1 + \frac{R'_{new}}{8T}} = 873,3 \text{ m}^2$$

$$a_{new} = \alpha_f \delta_f + \alpha_c \delta_c + \underbrace{\alpha_w (\delta_w - \delta_{abs})}_{\text{bare wall}} + \underbrace{\delta_{abs} \alpha_{abs}}_{\substack{\text{absorbing} \\ \text{material}}}$$

known  
↑

$$= a_{old} + \delta_{abs} (\alpha_{abs} - \alpha_w)$$

$$373, 3 \text{ m}^2 = 224 + \delta_{abs} (0.6 - 0.2)$$

$$a_{\text{new}} = \alpha_f \delta_f + \alpha_c \delta_c + \underbrace{\alpha_w (\delta_w - \delta_{\text{abs}})}_{\text{bare wall}} + \underbrace{\delta_{\text{abs}} \alpha_{\text{abs}}}_{\substack{\text{absorbing} \\ \text{material}}}$$

known  
↑

$$= a_{\text{old}} + \delta_{\text{abs}} (\alpha_{\text{abs}} - \alpha_w)$$

$$373, 3 \text{ m}^2 = 224 + \delta_{\text{abs}} (0.6 - 0.2)$$



$$S_{abs} = 373.3 \text{ m}^2$$

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impossible



because only  $320 \text{ m}^2$   
is available on walls!