

Magnetodynamic formulations and discretization



Magnetodynamics or magneto-quasi-statics (MQS)



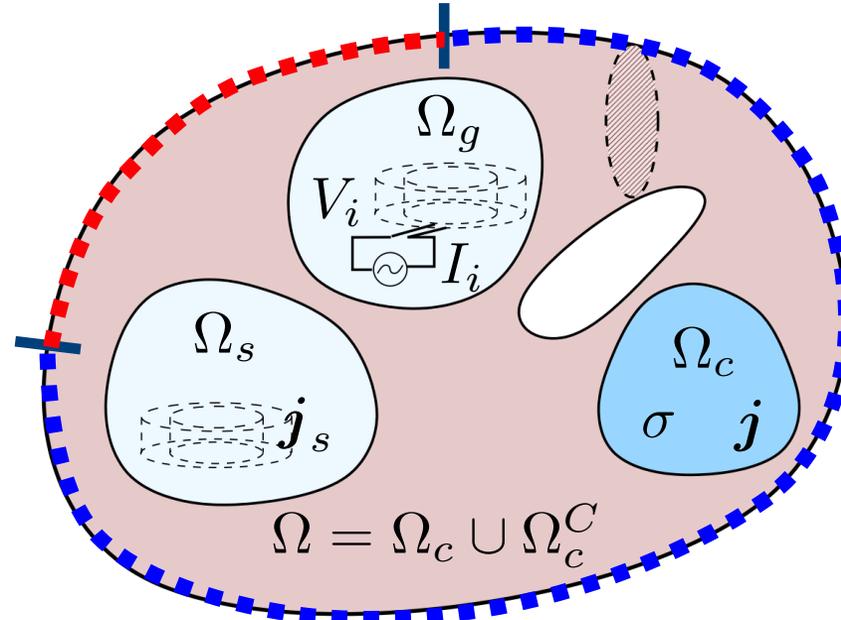
Distribution of magnetic field and eddy currents due to moving magnets and time variable sources

“*h* side”

Ampère’s law
verified in a
strong sense

h – φ formulation

t – ω formulation



“*b* side”

Faraday’s law
verified in a
strong sense

*a** formulation

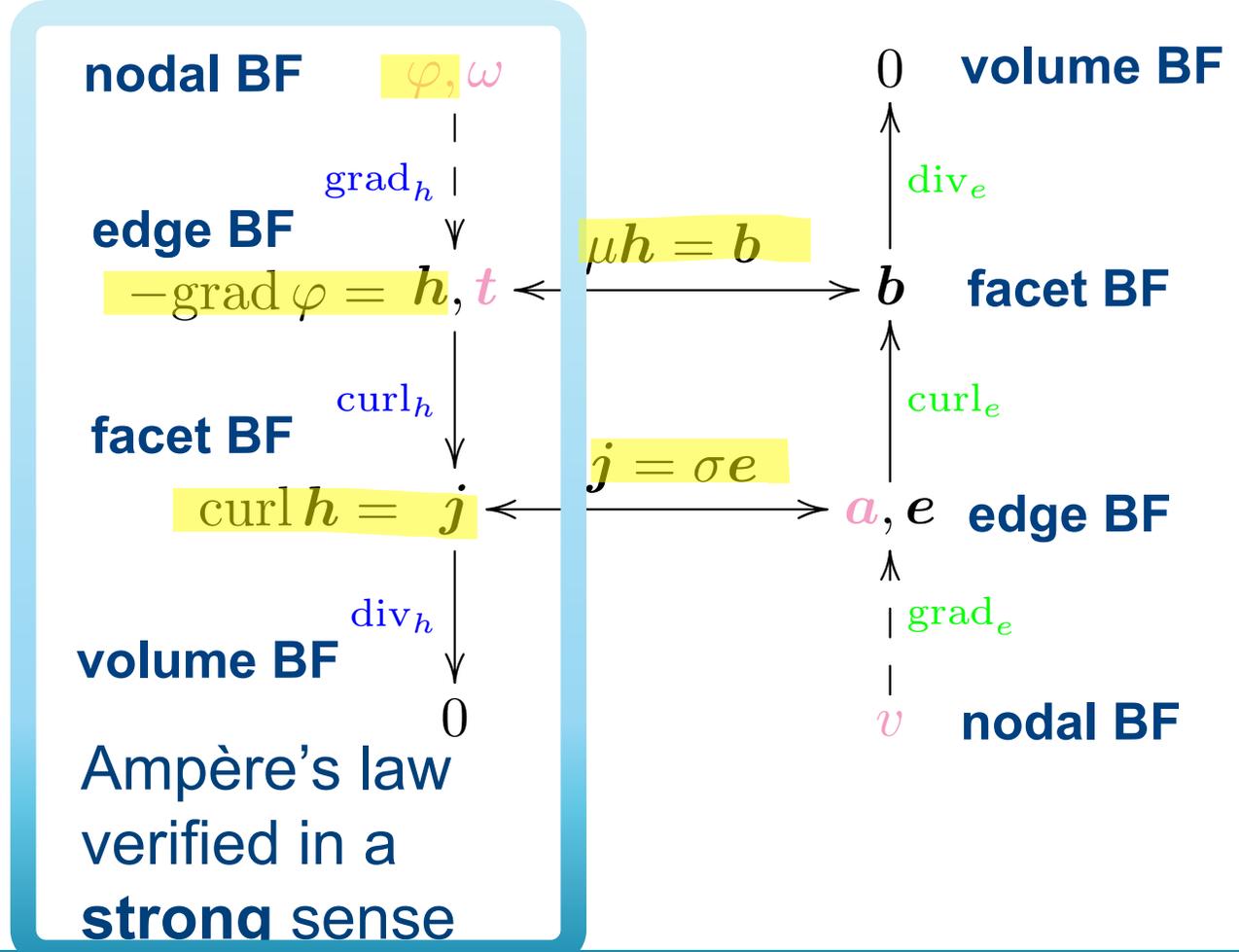
a – *v* formulation

$$\begin{aligned} \text{curl } \mathbf{h} &= \mathbf{j} & \mathbf{b} &= \mu \mathbf{h} (+\mathbf{b}_s) \\ \text{curl } \mathbf{e} &= -\partial_t \mathbf{b} & \mathbf{j} &= \sigma \mathbf{e} (+\mathbf{j}_s) \\ \text{div } \mathbf{b} &= 0 \end{aligned}$$

Displacement currents neglected with regard to eddy currents

Magnetodynamics

$$\text{curl } \mathbf{e} = -\partial_t \mathbf{b}, \quad \text{curl } \mathbf{h} = \mathbf{j}, \quad \text{div } \mathbf{b} = 0$$



$\mathbf{h} - \varphi$ formulation

\mathbf{h} magnetic field

φ magnetic scalar potential



resistivity $\rho = \frac{1}{\sigma}$

In non conduction domain:

$$\mathbf{h} = \mathbf{h}_s + \mathbf{h}_r \text{ with } \begin{cases} \text{curl } \mathbf{h}_s = \mathbf{j}_s \\ \text{curl } \mathbf{h}_r = 0 \end{cases}$$

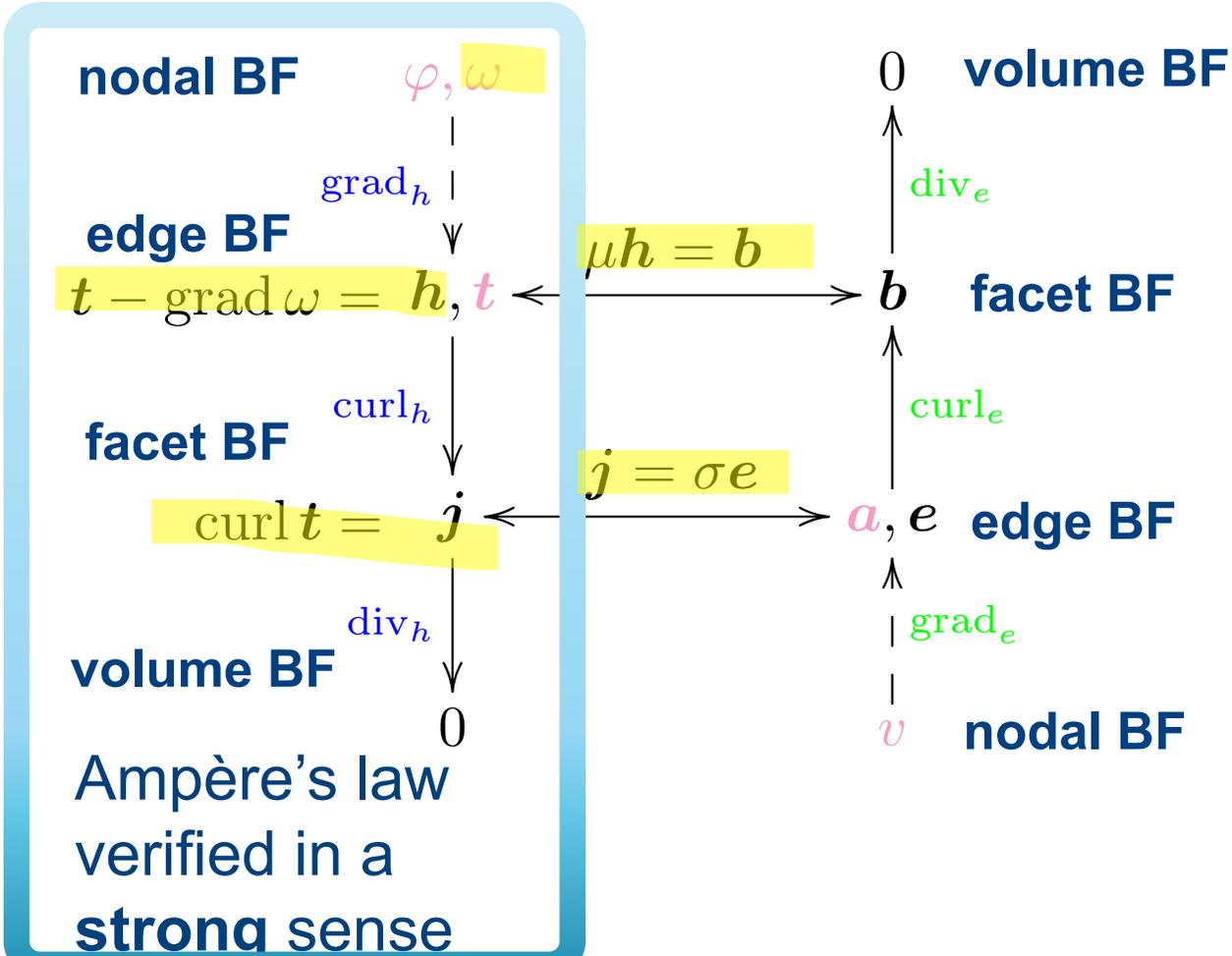
Faraday's law verified in a **weak** sense

$$\text{curl } \rho \text{ curl } \mathbf{h} + \partial_t (\mu \mathbf{h}) = 0 \text{ in } \Omega_c$$

$$\text{div} \left(\mu (\mathbf{h}_s - \text{grad } \varphi) \right) = 0 \text{ in } \Omega_c^C$$

Magnetodynamics

$$\text{curl } \mathbf{e} = -\partial_t \mathbf{b}, \quad \text{curl } \mathbf{h} = \mathbf{j}, \quad \text{div } \mathbf{b} = 0$$



$t - \omega$ formulation



t electric vector potential

ω magnetic scalar potential

resistivity $\rho = \frac{1}{\sigma}$

Faraday's law verified in a **weak sense**

+ Gauge in Ω

$$\text{curl} (\rho \text{curl } \mathbf{t}) + \partial_t (\mu(\mathbf{t} - \text{grad } \omega)) = 0 \quad \text{in } \Omega_c$$

$$\text{div} (\mu(\mathbf{t} - \text{grad } \omega)) = 0 \quad \text{in } \Omega_c^C$$

Magnetodynamics

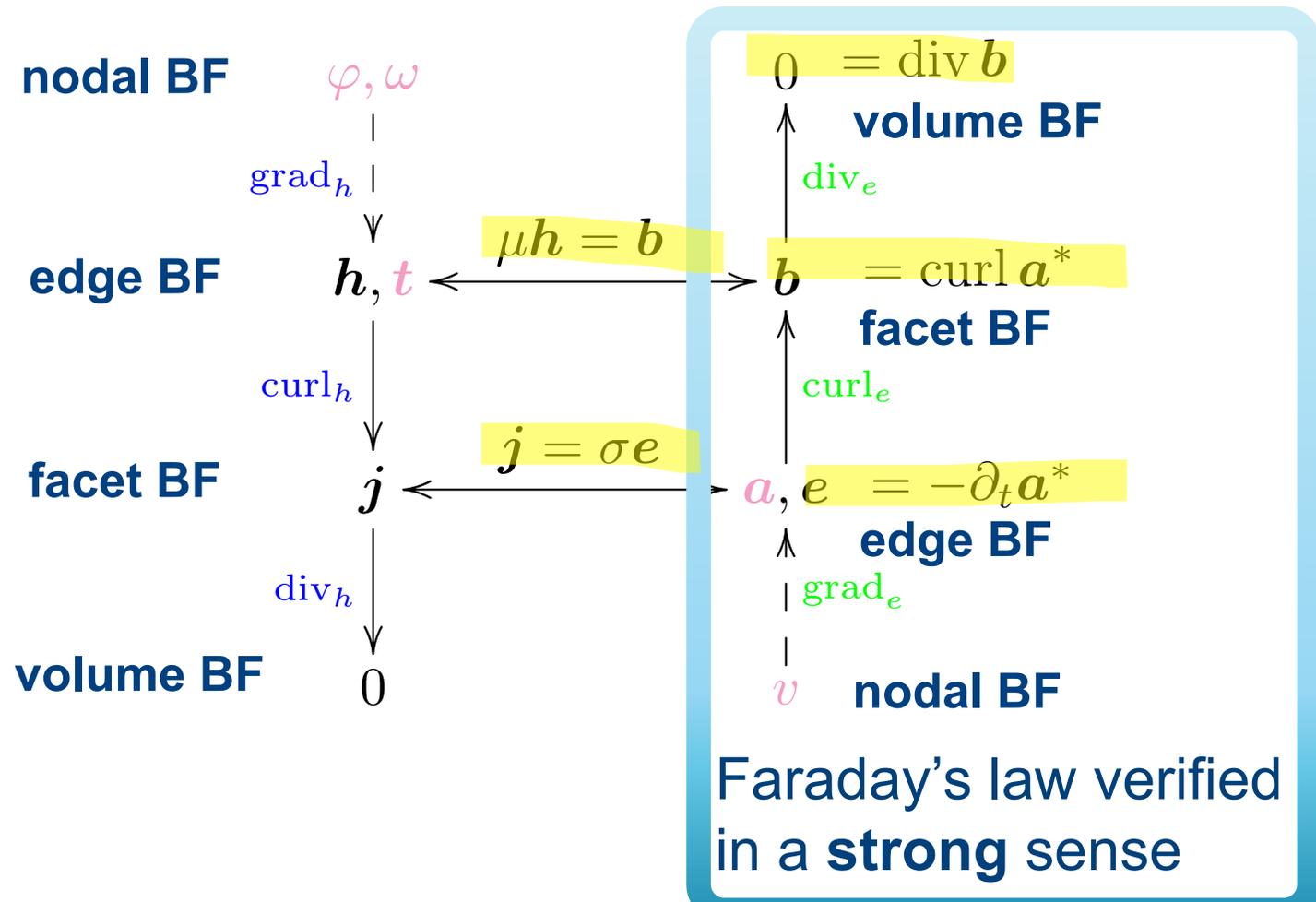
\mathbf{a}^* formulation



\mathbf{a}^* magnetic vector potential

$$\text{curl } \mathbf{e} = -\partial_t \mathbf{b}, \quad \text{curl } \mathbf{h} = \mathbf{j}, \quad \text{div } \mathbf{b} = 0$$

reluctivity $\nu = \frac{1}{\mu}$



Ampère's law verified in a **weak** sense

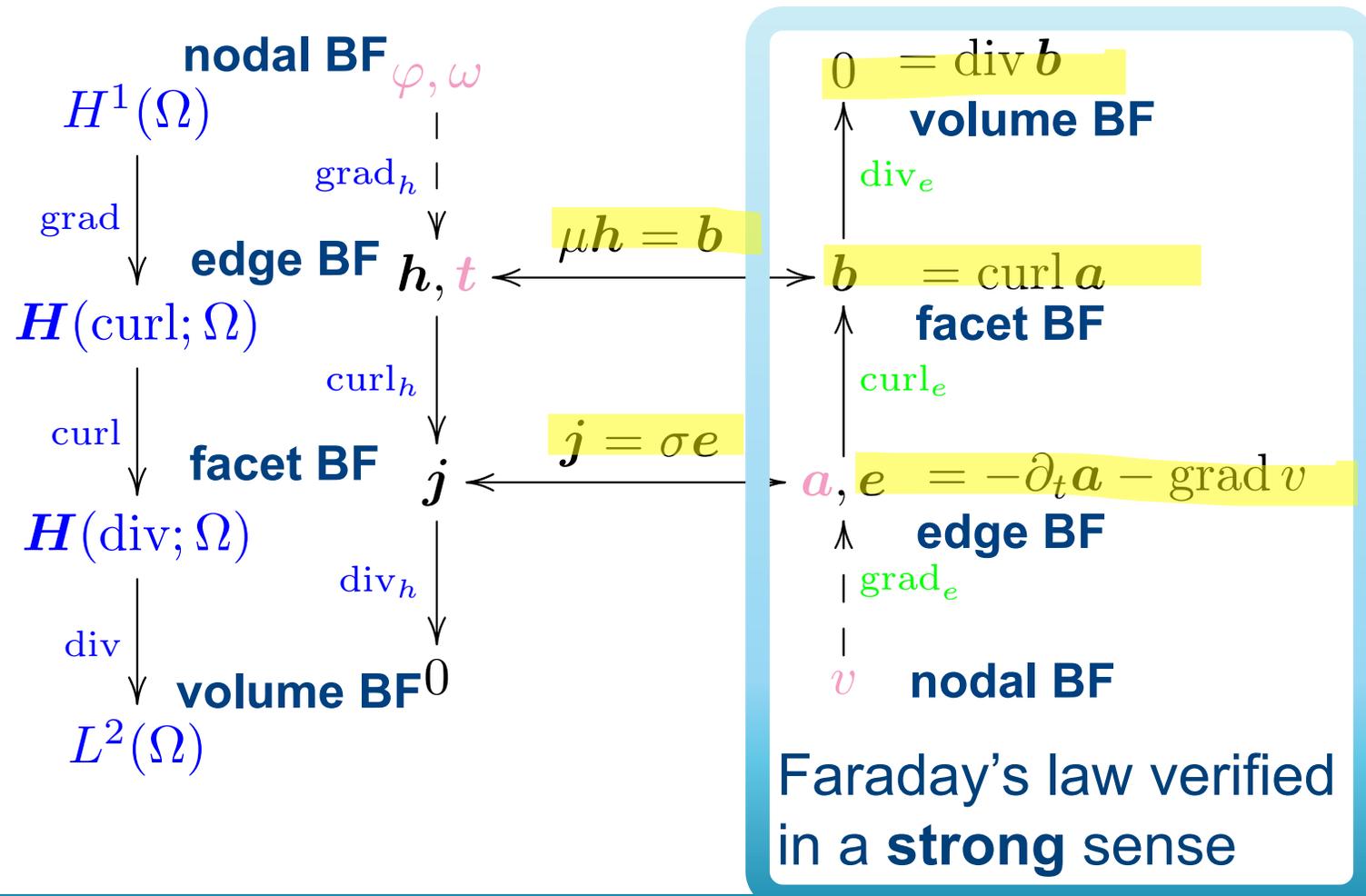
$$\text{curl } \nu \text{curl } \mathbf{a}^* + \sigma \partial_t \mathbf{a}^* = \mathbf{j}_s$$

+ Gauge in Ω_c^C

Magnetodynamics

$$\text{curl } \mathbf{e} = -\partial_t \mathbf{b}, \quad \text{curl } \mathbf{h} = \mathbf{j}, \quad \text{div } \mathbf{b} = 0$$

$\mathbf{a} - v$ formulation 
 \mathbf{a} magnetic vector potential
 v electric scalar potential potential



reluctivity $\nu = \frac{1}{\mu}$

Ampère's law verified in a **weak** sense

$$\text{curl } \nu \text{curl } \mathbf{a} + \sigma(\partial_t \mathbf{a} + \text{grad } v) = \mathbf{j}_s$$

$$\text{div} \left(-\sigma(\partial_t \mathbf{a} + \text{grad } v) \right) = 0 \quad \text{in } \Omega^C$$

+ Gauge in Ω

Spatial discretization — magnetodynamics

We want to find the modified magnetic vector potential $\mathbf{a}^*(\mathbf{x})$ in Ω

with given

$$\text{curl}(\nu \text{curl} \mathbf{a}^*) + \sigma \partial_t \mathbf{a}^* = \mathbf{j}_s$$

$\mathbf{j}_s(\mathbf{x})$ imposed electric current density

$\nu(\mathbf{x})$ reluctivity > 0 in part of the domain

$\sigma(\mathbf{x})$ sigma > 0 in part of the domain

$$\text{curl}(\nu \text{curl} \mathbf{a}^*) + \sigma \partial_t \mathbf{a}^* = \mathbf{j}_s$$

weighted residual approach

We integrate the equation weighted by (vectorial) weighting or test functions $\mathbf{w}_i(\mathbf{x})$ over the whole domain Ω :

find \mathbf{a}^* such that

$$\int_{\Omega} \left(\text{curl}(\nu \text{curl} \mathbf{a}^*) + \sigma \partial_t \mathbf{a}^* \right) \cdot \mathbf{w}_i \, d\Omega = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

holds $\forall \mathbf{w}_i$

Spatial discretization — magnetodynamics (II)

$$\int_{\Omega} \left(\operatorname{curl} (\nu \operatorname{curl} \mathbf{a}^*) + \sigma \partial_t \mathbf{a}^* \right) \cdot \mathbf{w}_i \, d\Omega = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

$$\begin{aligned} \mathbf{v} &= \mathbf{w}_i \\ \mathbf{u} &= \nu \operatorname{curl} \mathbf{a}^* \end{aligned}$$



$$\mathbf{v} \cdot \operatorname{curl} \mathbf{u} - \mathbf{u} \cdot \operatorname{curl} \mathbf{v} = \operatorname{div} (\mathbf{u} \times \mathbf{v})$$

integration by parts
Green formula

$$\int_{\Omega} \left(\operatorname{div} (\nu \operatorname{curl} \mathbf{a}^* \times \mathbf{w}_i) + \nu \operatorname{curl} \mathbf{a}^* \cdot \operatorname{curl} \mathbf{w}_i + \sigma \partial_t \mathbf{a}^* \cdot \mathbf{w}_i \right) d\Omega = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

$$\mathbf{u} = \nu \operatorname{curl} \mathbf{a}^* \times \mathbf{w}_i$$



$$\int_{\Omega} \operatorname{div} \mathbf{u} \, d\Omega = \oint_{\Gamma} \mathbf{u} \, d\Gamma, \quad d\Gamma = \mathbf{n} d\Gamma$$

divergence theorem

find \mathbf{a}^* such that

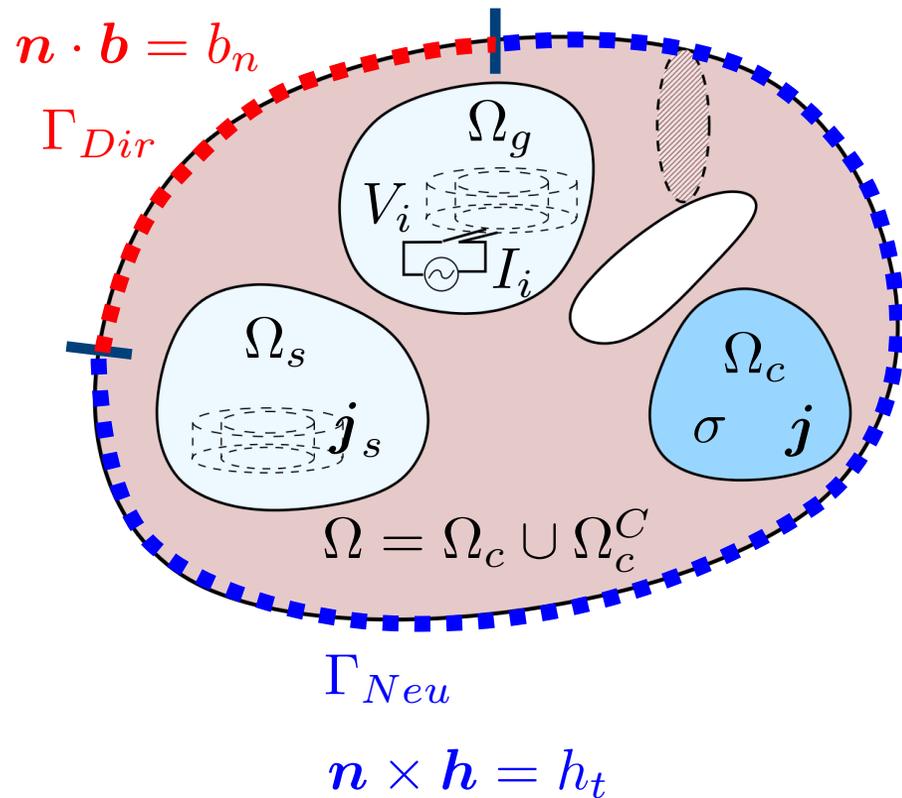
Weak formulation

$$\int_{\Gamma} (\nu \operatorname{curl} \mathbf{a}^* \times \mathbf{w}_i) \mathbf{n} d\Gamma + \int_{\Omega} \left(\nu \operatorname{curl} \mathbf{a}^* \cdot \operatorname{curl} \mathbf{w}_i + \sigma \partial_t \mathbf{a}^* \cdot \mathbf{w}_i \right) d\Omega = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

holds $\forall \mathbf{w}_i(\mathbf{x})$

only the first derivative of the MVP is now required

Spatial discretization — magnetodynamics (III)



Dirichlet BC at Γ_{Dir}

$$\mathbf{a}^* \times \mathbf{n} = \mathbf{a}_{Dir}^* \times \mathbf{n} \iff \mathbf{b} \cdot \mathbf{n} = b_n$$

Homogeneous Neumann BC at Γ_{Neu}

$$h_t = \nu \operatorname{curl} \mathbf{a}^* \times \mathbf{n} = 0$$

$$\underbrace{\int_{\Gamma_{Dir}} (\nu \operatorname{curl} \mathbf{a}^* \times \mathbf{w}_i) \mathbf{n} d\Gamma}_{= 0} + \underbrace{\int_{\Gamma_{Neu}} (\nu \operatorname{curl} \mathbf{a}^* \times \mathbf{w}_i) \mathbf{n} d\Gamma}_{= 0}$$

$$\forall \mathbf{w}_i(\mathbf{x}) : \mathbf{w}_i \times \mathbf{n} = 0$$

essential BC

natural BC

Spatial discretization — magnetodynamics (IV)

$$\mathbf{a}^*(\mathbf{x}) \approx \mathbf{a}_h^*(\mathbf{x}) = \sum_{j=1}^N u_j \mathbf{s}_j$$

$$\mathbf{s}_j(\mathbf{x}) \times \mathbf{n} = 0 \text{ at } \Gamma_{Dir}$$

$$\begin{cases} \mathbf{s}_j(\mathbf{x}) & \text{shape functions} \\ u_j & \text{scalar unknowns, Dofs} \end{cases}$$

Ritz-Galerkin method

$$\mathbf{s}_j(\mathbf{x}) = \mathbf{w}_j(\mathbf{x})$$

Petrov-Galerkin method

$$\mathbf{s}_j(\mathbf{x}) \neq \mathbf{w}_j(\mathbf{x})$$

$$\int_{\Omega} \left(\nu \operatorname{curl} \mathbf{a}^* \cdot \operatorname{curl} \mathbf{w}_i + \sigma \partial_t \mathbf{a}^* \cdot \mathbf{w}_i \right) d\Omega = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i d\Omega$$



$$\sum_j \left(u_j \underbrace{\int_{\Omega} \nu \operatorname{curl} \mathbf{w}_j \cdot \operatorname{curl} \mathbf{w}_i d\Omega}_{= k_{ij}} + \partial_t u_j \underbrace{\int_{\Omega} \sigma \mathbf{w}_j \cdot \mathbf{w}_i d\Omega}_{= m_{ij}} \right) = \underbrace{\int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i d\Omega}_{= f_i}$$



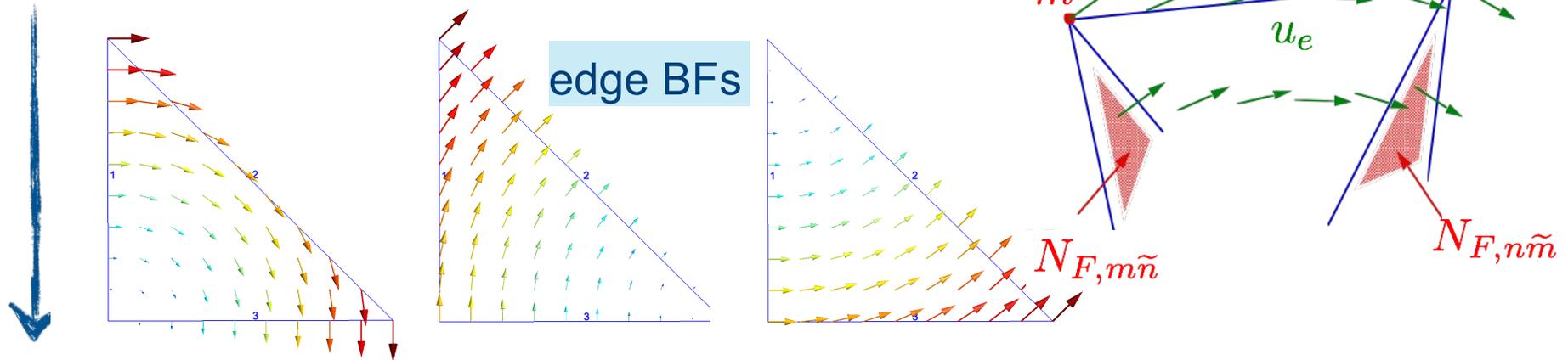
$$[k_{ij}][u_j] + [m_{ij}][\partial_t u_j] = [f_i]$$

K and M symmetric, semi-positive-definite

Spatial discretization — magnetodynamics (V)

$$\sum_j \left(u_j \int_{\Omega} \nu \operatorname{curl} \mathbf{w}_j \cdot \operatorname{curl} \mathbf{w}_i \, d\Omega + \partial_t u_j \int_{\Omega} \sigma \mathbf{w}_j \cdot \mathbf{w}_i \, d\Omega \right) = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

$$\operatorname{curl} \mathbf{w}_j = \sum_q c_{jq} \mathbf{z}_q$$



$$\sum_j \left(u_j \underbrace{\sum_p \sum_q c_{ip} c_{jq}}_{\mathbf{A}_j} \int_{\Omega} \nu \mathbf{z}_q \cdot \mathbf{z}_p \, d\Omega + \partial_t u_j \int_{\Omega} \sigma \mathbf{w}_j \cdot \mathbf{w}_i \, d\Omega \right) = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

\mathbf{A}_j \mathcal{M}_{pq}^ν \mathcal{M}_{ij}^σ \mathcal{J}_i^s

$$\text{FE matrix system } \tilde{\mathcal{C}} \mathcal{M}^\nu \mathcal{C} \mathbf{A} + \mathcal{M}^\sigma \partial_t \mathbf{A} = \mathcal{J}^s$$

Inserting boundary conditions

unconstraint system

$$\begin{bmatrix} \mathbf{K}_{bb} & \mathbf{K}_{bc} \\ \mathbf{K}_{cb} & \mathbf{K}_{cc} \end{bmatrix} \begin{bmatrix} \mathbf{u}_b \\ \mathbf{u}_c \end{bmatrix} = \begin{bmatrix} \mathbf{f}_b \\ \mathbf{f}_c \end{bmatrix}$$

potentials living at Dirichlet boundaries

adding constraints leads to

$$\begin{bmatrix} \mathbf{K}_{bb} & \mathbf{K}_{bc} & 0 \\ \mathbf{K}_{cb} & \mathbf{K}_{cc} & \mathbf{B}_{cq} \\ 0 & \mathbf{B}_{qc} & 0 \end{bmatrix} \begin{bmatrix} \mathbf{u}_b \\ \mathbf{u}_c \\ \mathbf{y}_q \end{bmatrix} = \begin{bmatrix} \mathbf{f}_b \\ \mathbf{f}_c \\ 0 \end{bmatrix}$$

eliminate known potentials

$$\mathbf{K}_{bb}\mathbf{u}_b = \mathbf{f}_b - \mathbf{K}_{bc}\mathbf{u}_c$$

$$[\mathbf{K}_{bb}] [\mathbf{u}_b] = [\mathbf{f}_b - \mathbf{K}_{bc}\mathbf{u}_c]$$

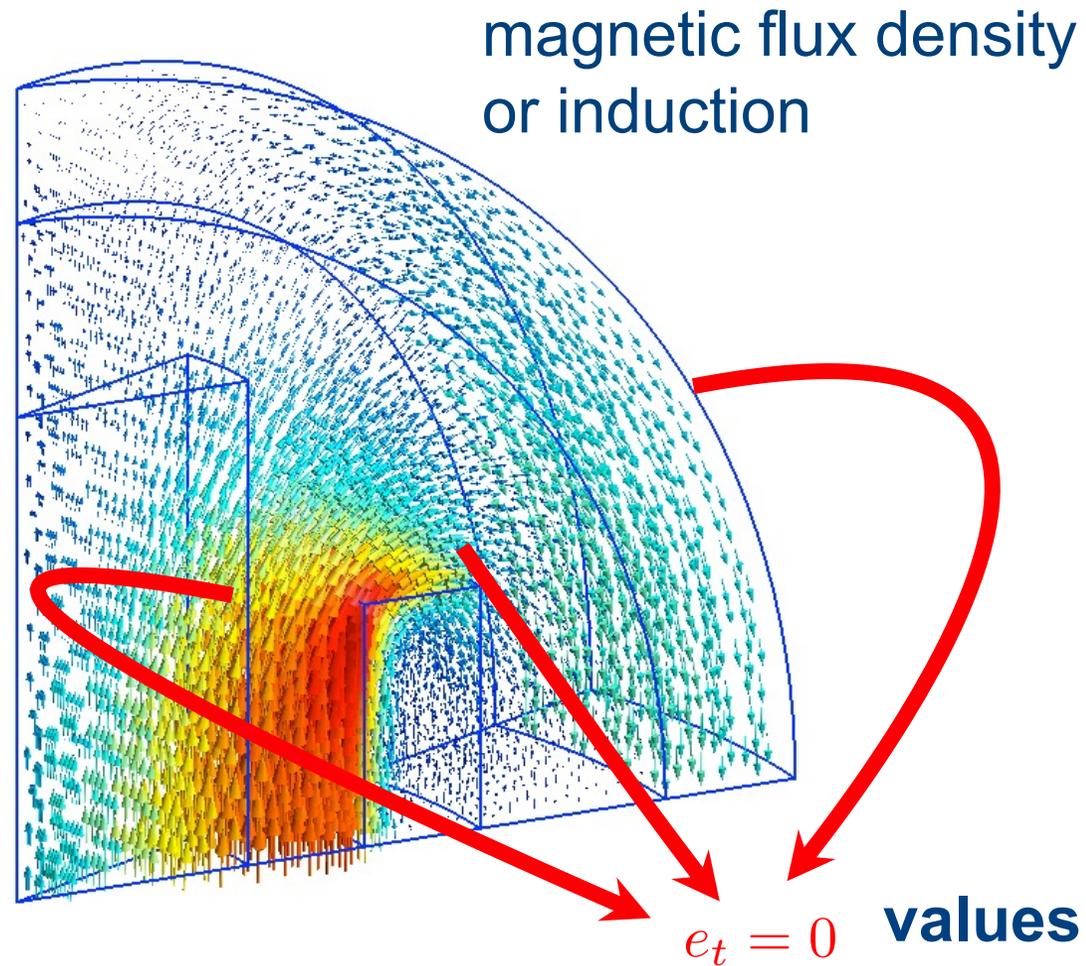
matrix system is shrank

Boundary conditions

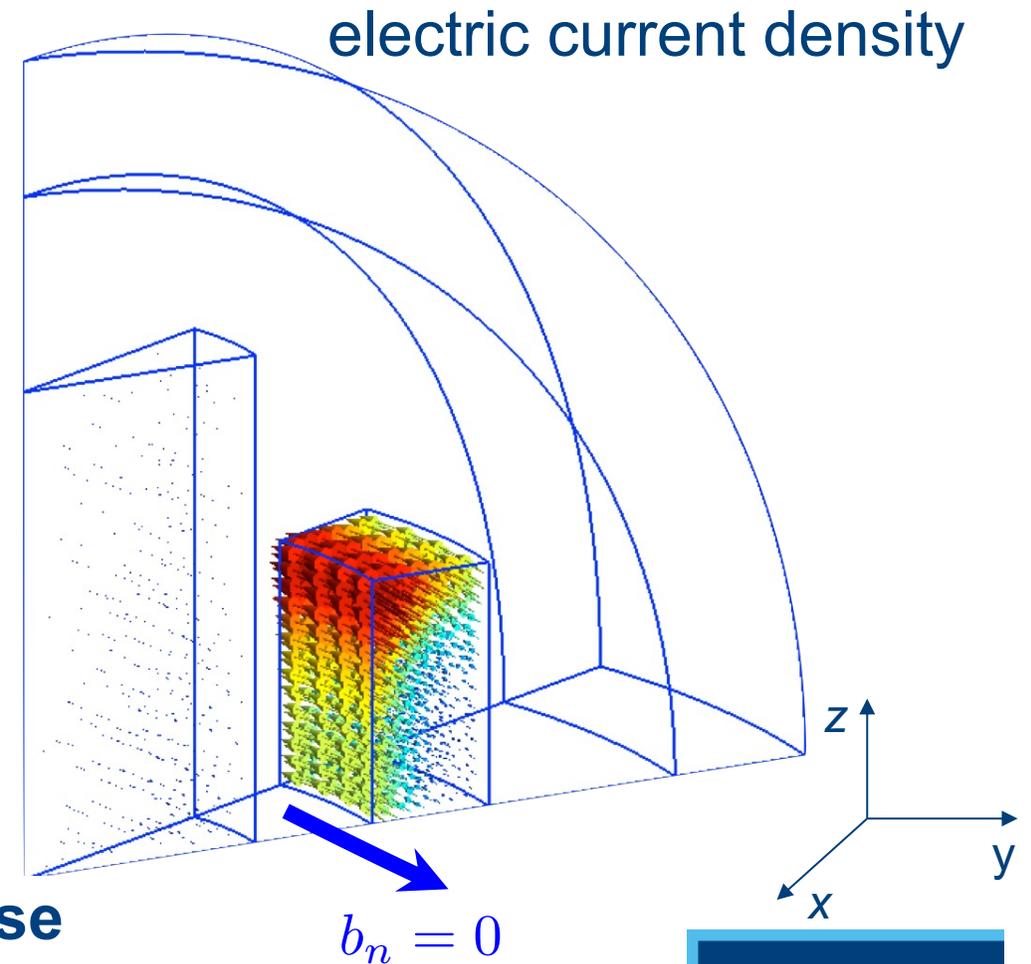
Duality between formulations

	electric BC “flux wall” “current gate”	magnetic BC “flux gate” “current wall”
definition	\mathbf{e}_t	\mathbf{h}_t
electric current	$\mathbf{j}_n \neq 0$	$\mathbf{j}_n = 0$
magnetic flux	$\mathbf{b}_n = 0$	$\mathbf{b}_n \neq 0$
magnetic vector <i>b</i> -conform potential formulation	Dirichlet BC	Neumann BC
magnetic scalar <i>h</i> -conform potential formulation	Neumann BC	Dirichlet BC

Boundary conditions (II)



values to impose
at symmetry planes



From 3D to 2D models

$$\mathbf{j} = (0, 0, j_z(\mathbf{x}))$$

$$\mathbf{b} = (b_x(\mathbf{x}), b_y(\mathbf{x}), 0)$$

$$\mathbf{h} = (h_x(\mathbf{x}), h_y(\mathbf{x}), 0)$$

$$\mathbf{a} = (0, 0, a_z(\mathbf{x}))$$

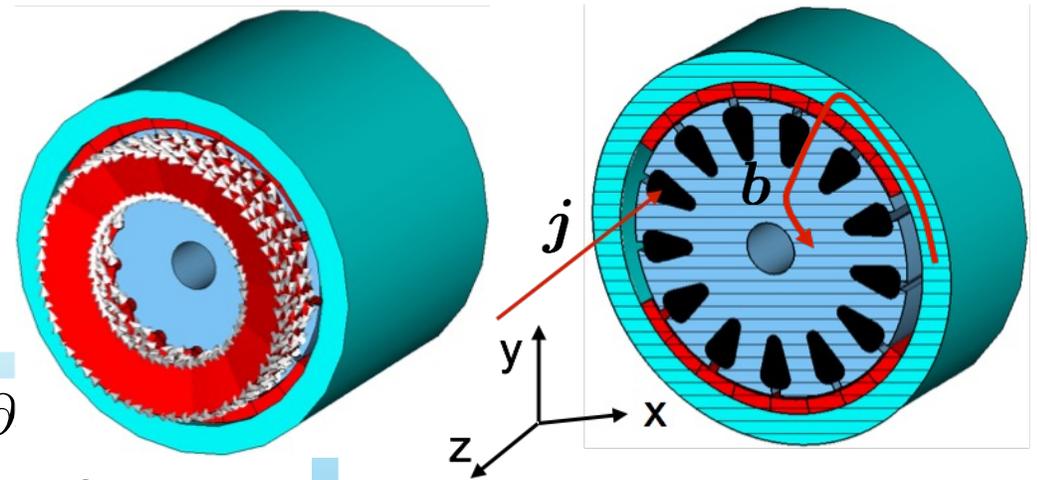
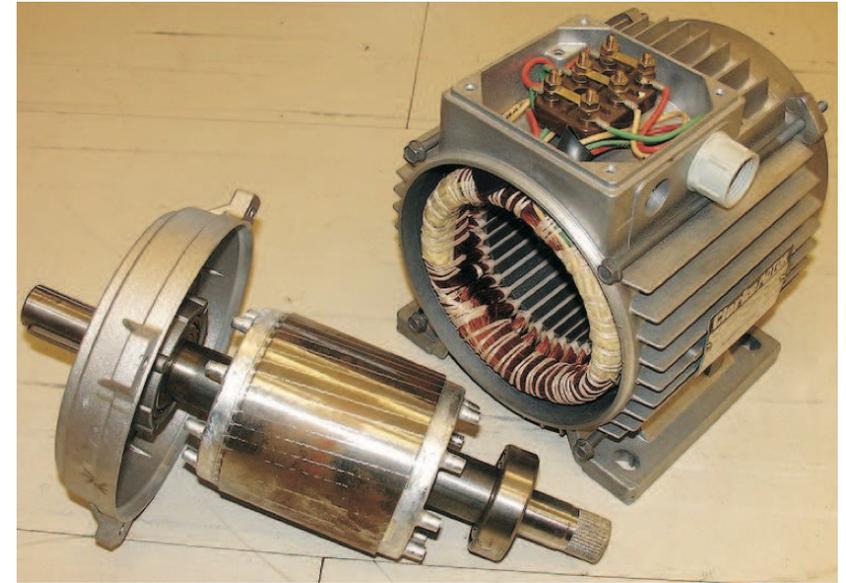
$$\mathbf{b} = \text{curl } \mathbf{a} = (\partial_y a_z, -\partial_x a_z, 0)$$

$$\mathbf{h} = \nu \text{curl } \mathbf{a} = \nu (\partial_y a_z, -\partial_x a_z, 0)$$

$$\mathbf{j} = (0, 0, \partial_x h_y - \partial_y h_x) = (0, 0, j_{s,z} - \sigma \partial_t a_z)$$

$$\text{div } \mathbf{b} = \partial_x b_x + \partial_y b_y = \partial_{xy}^2 a_z - \partial_{xy}^2 a_z = 0$$

$$-\partial_x(\nu \partial_x a_z) - \partial_y(\nu \partial_y a_z) + \sigma \partial_t \text{curl}(\nu \text{curl } \mathbf{a}) + \sigma \partial_t \mathbf{a} = \mathbf{j}_s$$

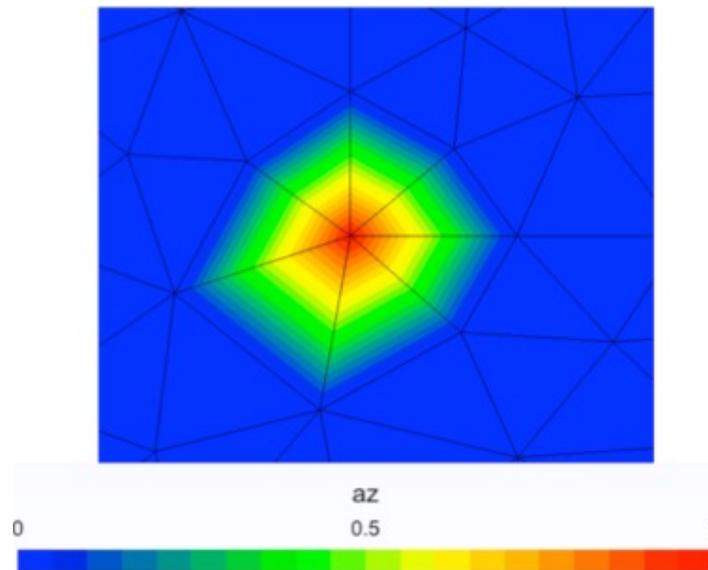
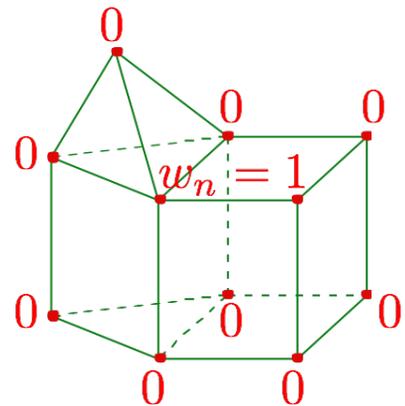


2D spatial discretization

$$\sum_j \left(u_j \int_{\Omega} \nu \operatorname{curl} \mathbf{w}_j \cdot \operatorname{curl} \mathbf{w}_i \, d\Omega + \partial_t u_j \int_{\Omega} \sigma \mathbf{w}_j \cdot \mathbf{w}_i \, d\Omega \right) = \int_{\Omega} \mathbf{j}_s \cdot \mathbf{w}_i \, d\Omega$$

$$\mathbf{a} = \sum_j u_j \mathbf{w}_{e,j} = \sum_j u_j \frac{w_{n,j}(\mathbf{x})}{l_z} \hat{\mathbf{z}}$$

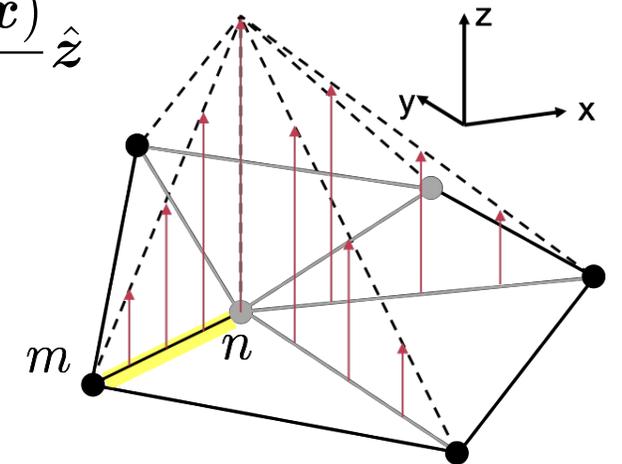
$$\mathbf{a}(\mathbf{x}_n) = \frac{u_n}{l_z} \hat{\mathbf{z}}$$



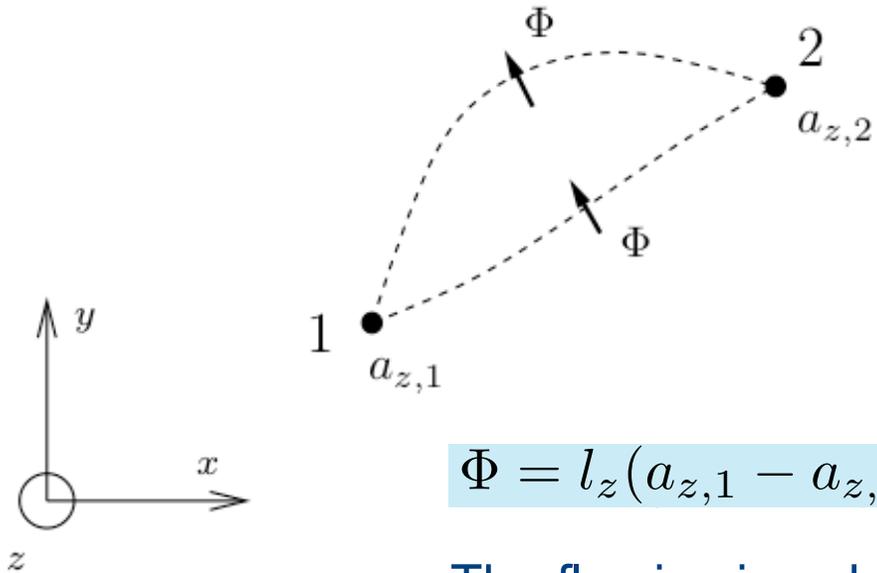
$$\mathbf{w}_e = \varsigma_m \operatorname{grad} \varsigma_n - \varsigma_n \operatorname{grad} \varsigma_m$$

$$w_n = \varsigma_n$$

$$\mathbf{w}_e = \frac{w_n(\mathbf{x})}{l_z} \hat{\mathbf{z}}$$

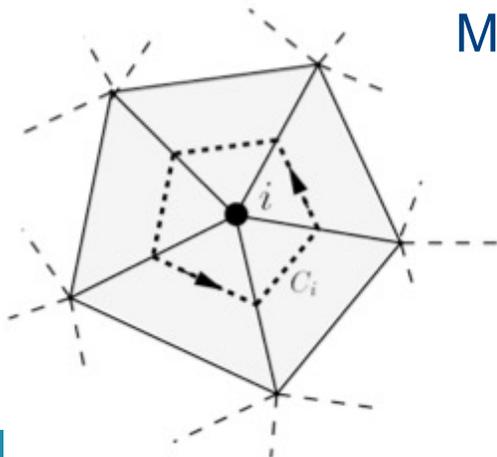


Physical meaning of MVP & FE equations

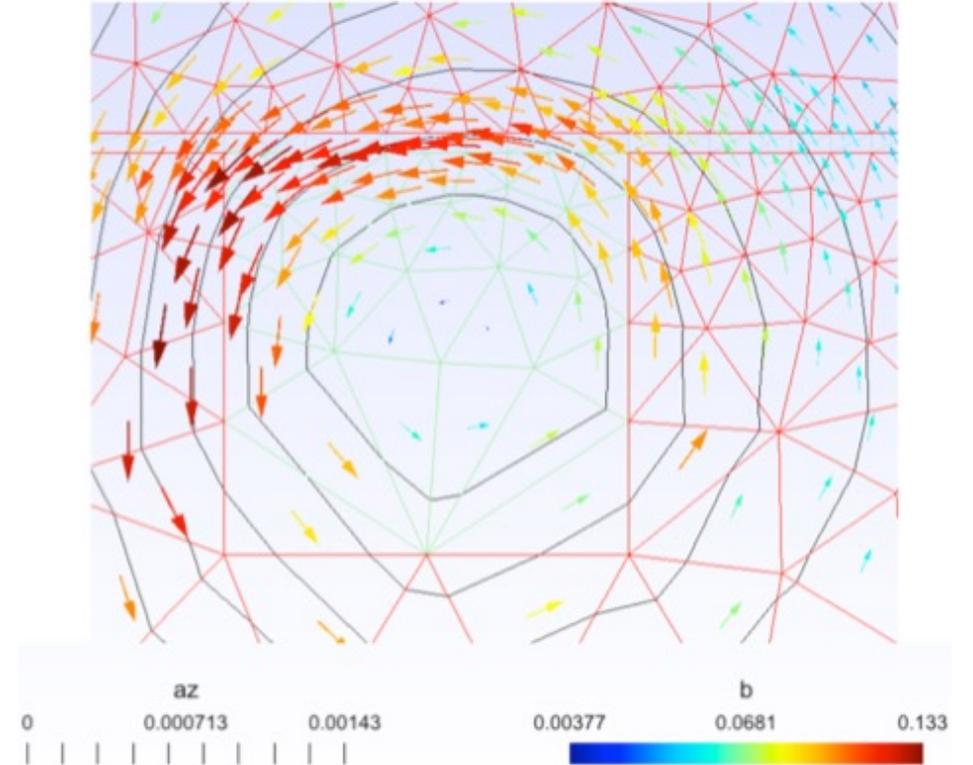


$$\Phi = l_z(a_{z,1} - a_{z,2})$$

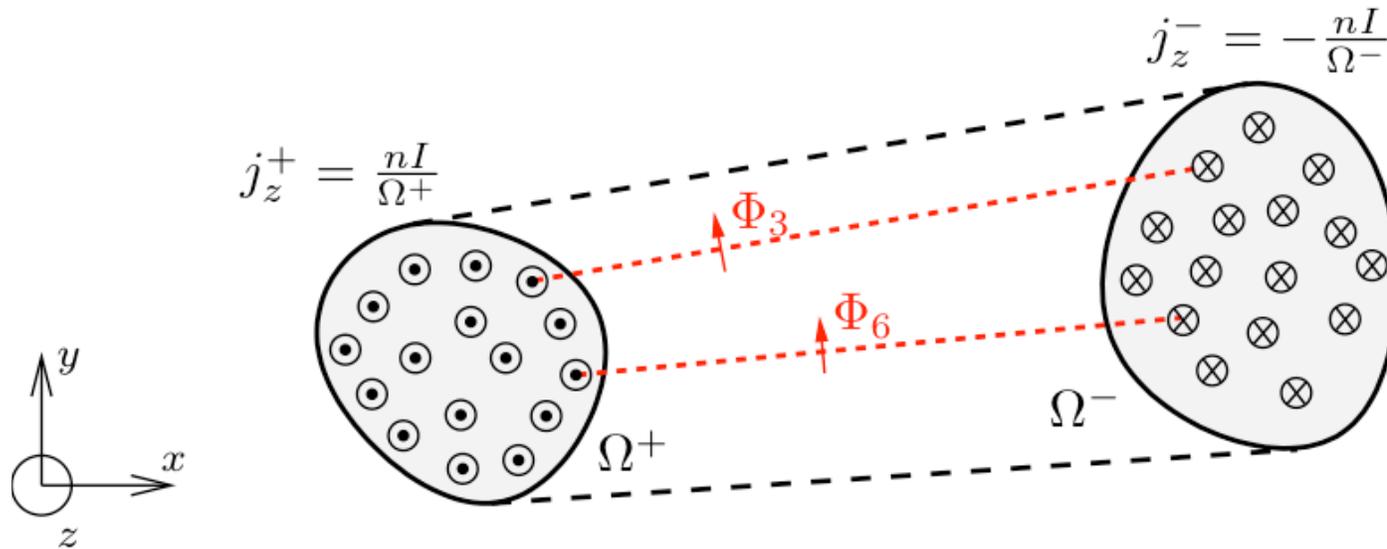
The flux is given by difference of z-MVPs multiplied by the axial length



$$\int_{\Omega} \mathbf{h} \cdot \text{curl} \mathbf{w}_i \, d\Omega = \oint_{C_i} \mathbf{h} \cdot d\mathbf{l} = 0$$



Flux and flux linkage of a coil



Coil with $n=16$ turns with two coil sides (+,-)

Flux of two turns is depicted
Current density, I/A

$$\Phi = \sum_{k=1}^n \Phi_k \quad \text{Total flux-linkage of the coil (Vs or Wb)}$$

$$j_z = \pm \frac{nI}{\Omega^\pm} \text{ in } \Omega_{\text{coil}} = \Omega^+ \cup \Omega^-$$

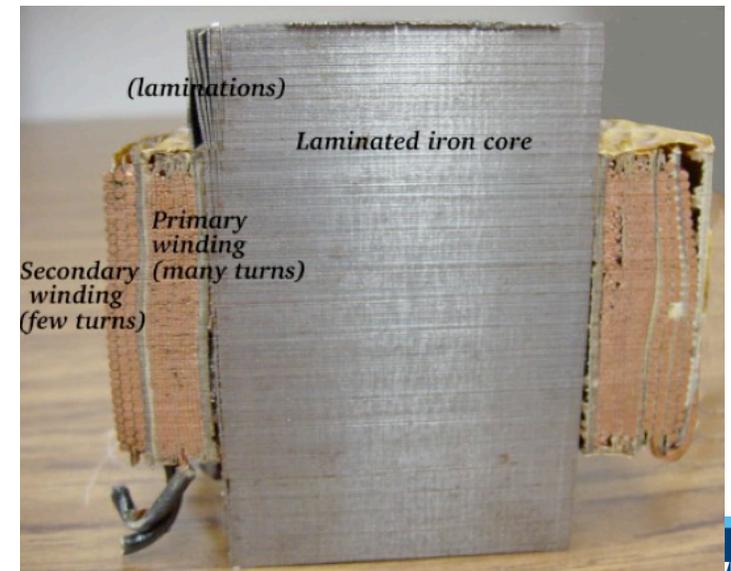
uniform current region
per coil-side region, i.e.
homogenisation

$$j_{z,1A} = \pm \frac{n}{\Omega^\pm} \text{ in } \Omega_{\text{coil}} = \Omega^+ \cup \Omega^-$$

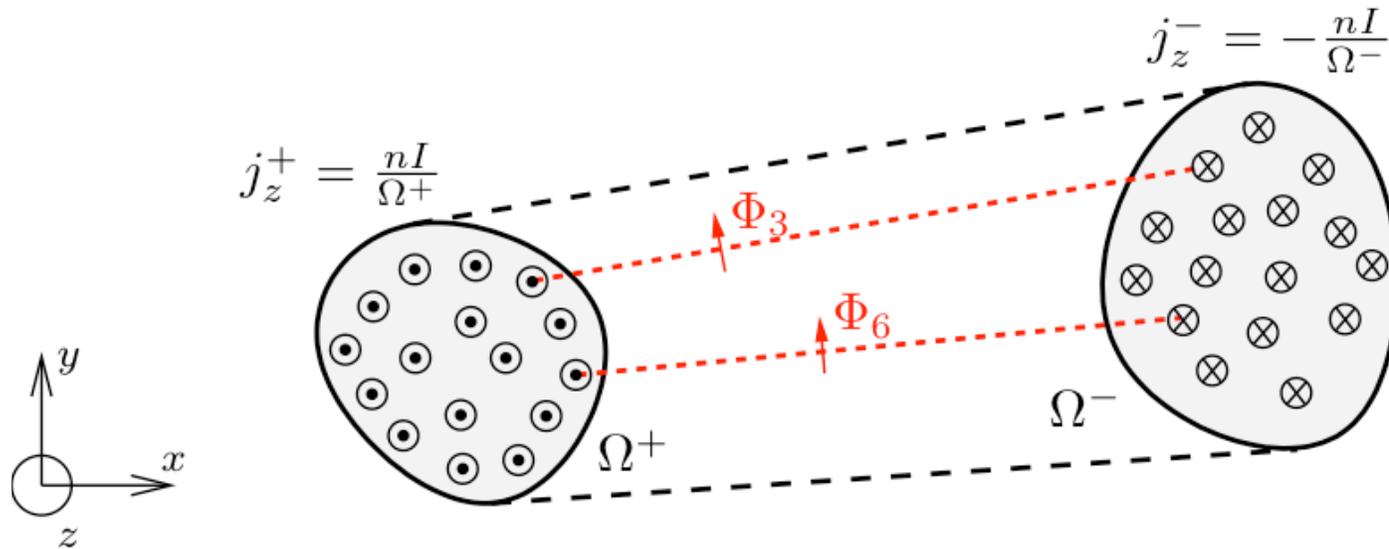
homogenised
1D current density ($1/m^2$)

$$\Psi = l_z \int_{\Omega_{\text{coil}}} a_z j_{z,1A} d\Omega$$

flux-linkage (in Vs) from a
FE solution in terms of MVP



Flux and flux linkage of a coil



$$j_{z,1A} = \pm \frac{n}{\Omega^\pm} \text{ in } \Omega_{\text{coil}} = \Omega^+ \cup \Omega^-$$

$$\Psi = l_z \int_{\Omega_{\text{coil}}} a_z j_{z,1A} d\Omega$$

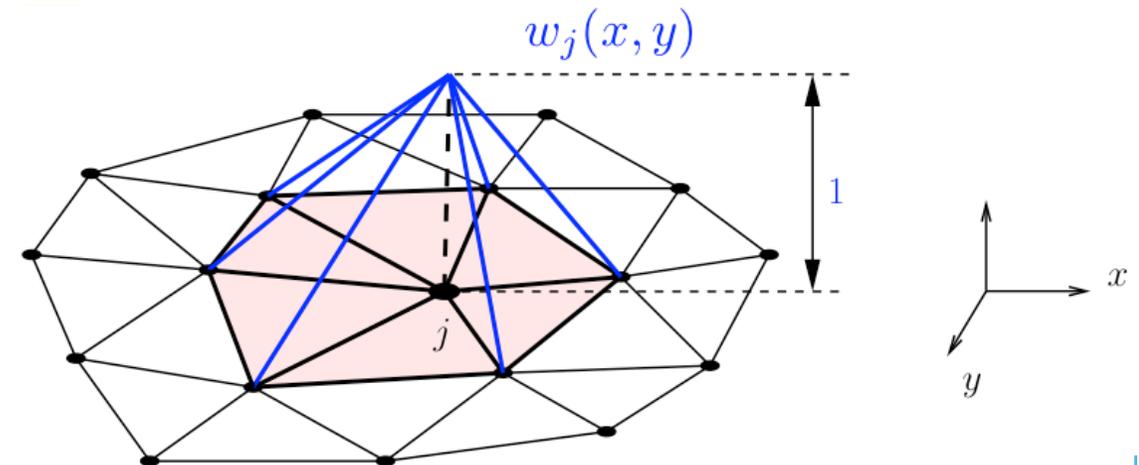
$$\mathbf{S} \mathbf{A} = \mathbf{J}$$

$$j_z = j_{z,1A} I$$

$$\mathbf{J}_i = \int_{\Omega} \mathbf{j} \cdot \mathbf{w}_i d\Omega$$

$$\mathbf{S} \mathbf{A} = \mathbf{K} I$$

$$\mathbf{K}_i = \int_{\Omega} j_{z,1A} w_i d\Omega$$



2D Coil model — example electrical machine

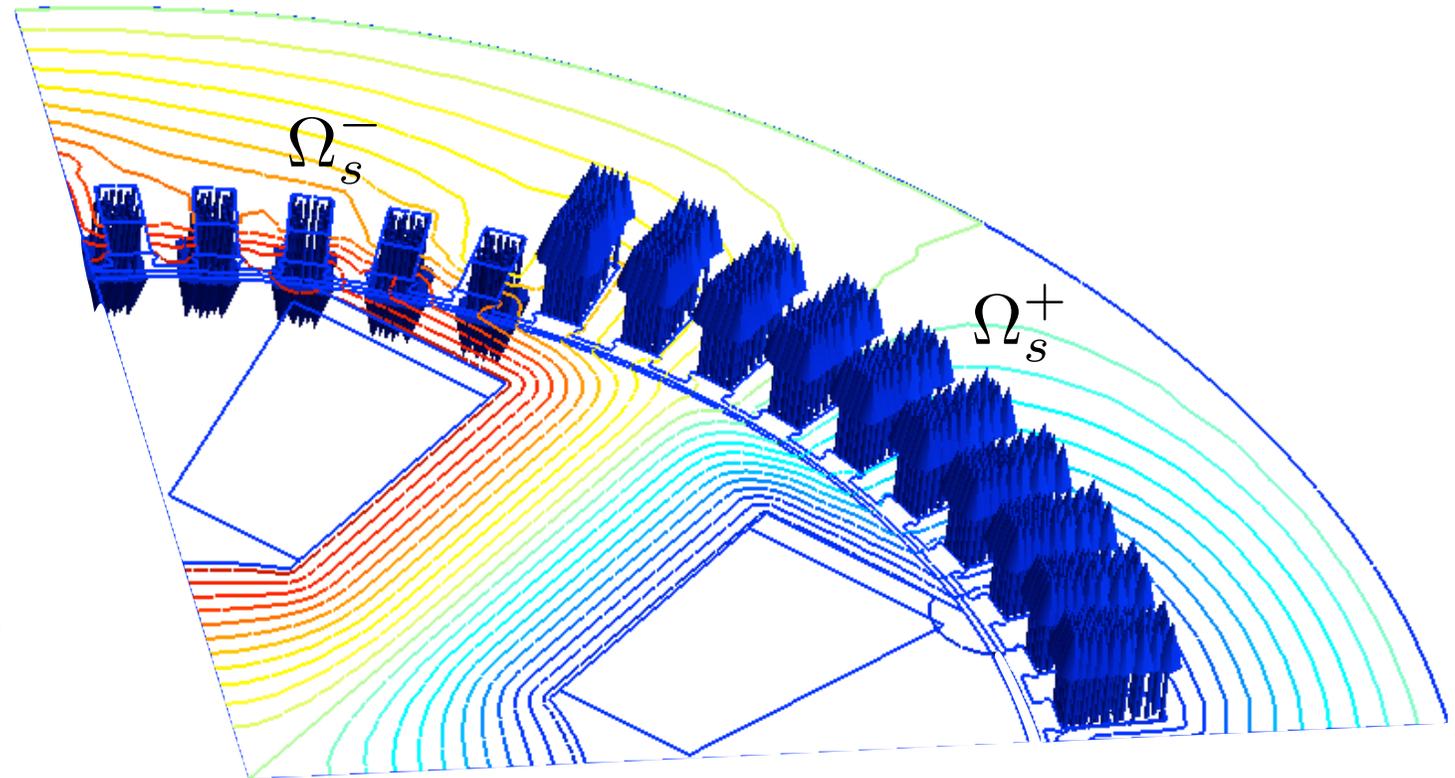
with S the area of the slot
and N_i the number of turns of the winding

$$\mathbf{j} = (0, 0, j_z)$$

$$\mathbf{t}_{\Omega_s^+} = \frac{N_i}{S} \hat{\mathbf{z}}$$

$$\mathbf{t}_{\Omega_s^-} = -\frac{N_i}{S} \hat{\mathbf{z}}$$

$$\begin{aligned} \Psi &= \int_{\Omega_s} \mathbf{a} \cdot \hat{\mathbf{t}} \, dS \\ &= \frac{N_i}{S} \int_{\Omega_s^+} a_z \, dS - \frac{N_i}{S} \int_{\Omega_s^-} a_z \, dS \end{aligned}$$



Coil model (cont'd)

induced voltage \sim flux linkage

what flux is linked?

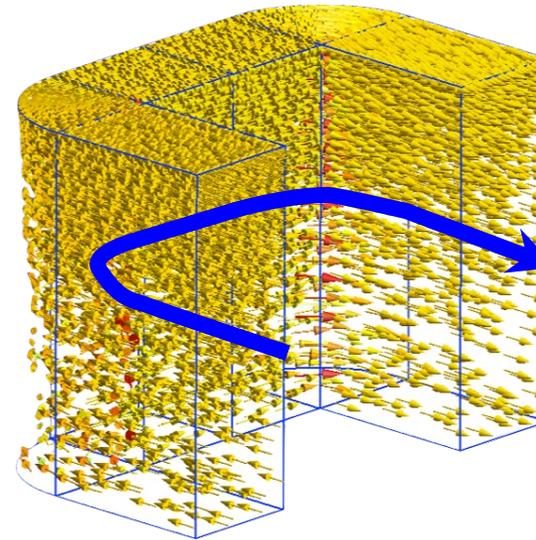
for a single path $\Phi = \oint_{\gamma} \mathbf{a} \cdot d\mathbf{l}$

for a coil

- ✓ integrating along the coil
- ✓ average of the coil cross-section

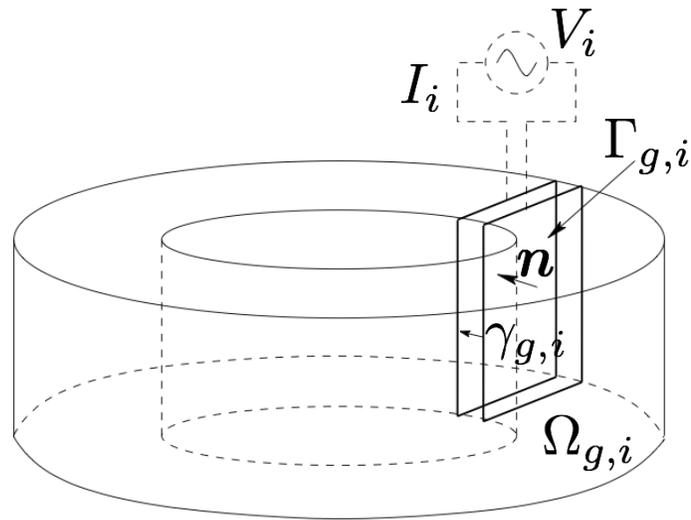
$$\Psi = \frac{n}{S_{coil}} \int_{S_{coil}} \mathbf{a} \cdot \hat{\mathbf{t}} \, dS$$

$\hat{\mathbf{t}}$ current direction vector



$\hat{\mathbf{t}}$ tangent vector
from geometry

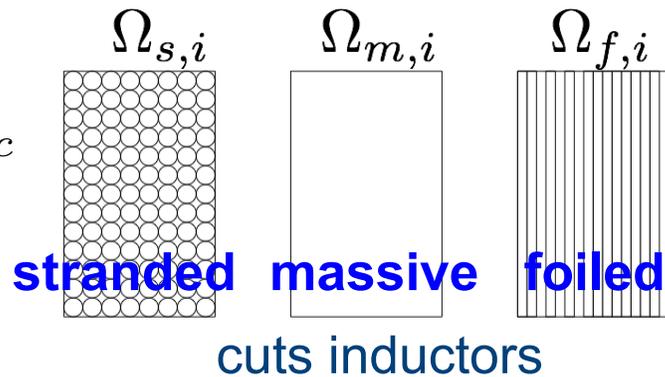
Coil model



sources in

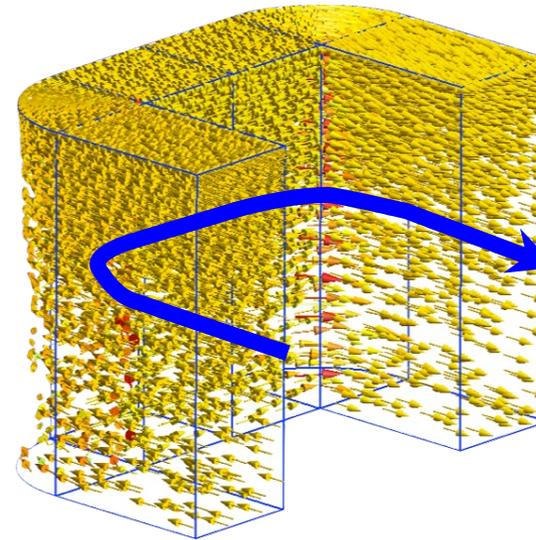
$$\Omega_s \in \Omega_c^C$$

$$\Omega_m, \Omega_f \in \Omega_c$$



stranded inductors (N_i turns) $\Omega_s \in \Omega_c^C$

✓ imposed current density $\mathbf{j}_s = i_s(t) \hat{\mathbf{t}}$

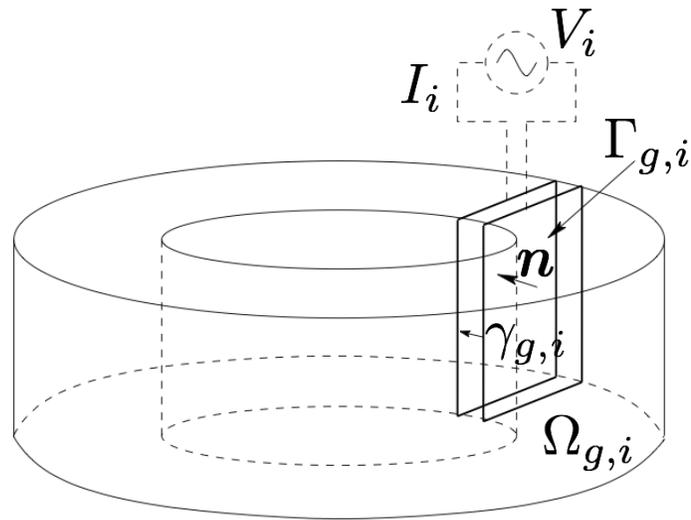


$\hat{\mathbf{t}}$ tangent vector
from geometry

✓ imposed current or voltage
 $\Rightarrow \mathbf{j}_s$ unknown

$$\begin{cases} \text{curl } \mathbf{h}_s = \mathbf{j}_s & \text{in } \Omega_s \\ \text{curl } \mathbf{h}_s = 0 & \text{in } \Omega_s^C \end{cases} \quad \begin{array}{l} \mathbf{h}_s \text{ computed via FEs} \\ \mathbf{h}_s \text{ not unique} \end{array}$$

Coil model (cont'd)



massive inductors $\Omega_m \in \Omega_c$

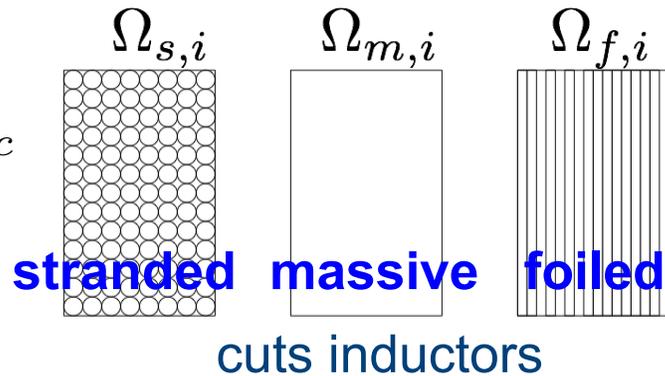
$$\int_{\gamma_{g,i}} \mathbf{e} \cdot d\mathbf{l} = V_i$$

$$\int_{\Gamma_{g,i}} \mathbf{n} \cdot \mathbf{j} \, ds = I_i$$

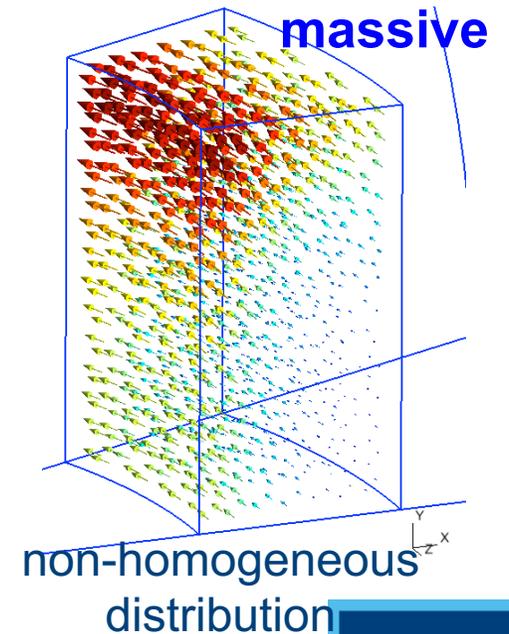
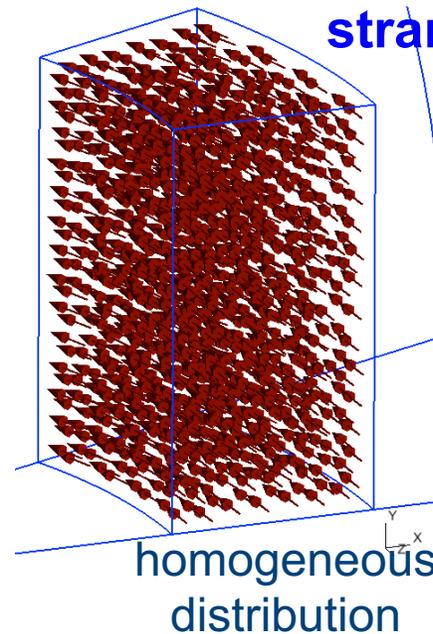
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$$\Omega_s \in \Omega_c^C$$

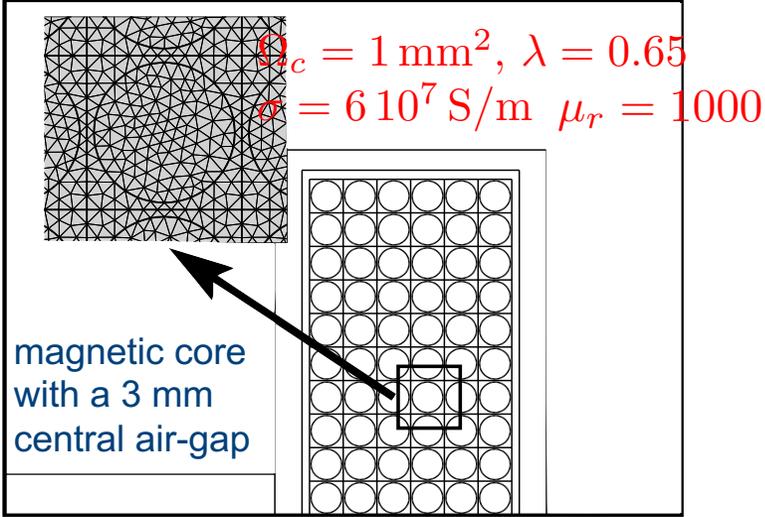
$$\Omega_m, \Omega_f \in \Omega_c$$



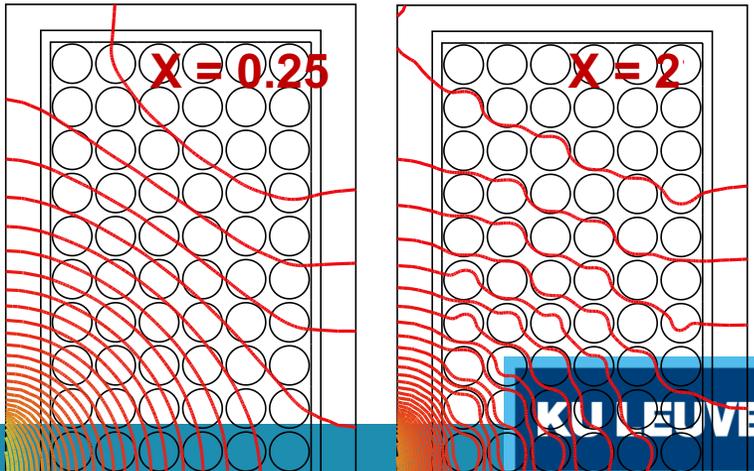
cuts inductors



Multi-turn windings and eddy current effects



significant EC effect, affecting visibly the flux lines



Homogenization methods are indispensable!

Multi-turn windings and eddy-current effects: Skin and proximity effects

The *equivalent radius* of the conductors, of arbitrary but symmetrical cross-sectional shape, is given by $r = \sqrt{\Omega_c/\pi}$, where Ω_c is the cross-sectional surface area. The skin depth at frequency f or pulsation $\omega = 2\pi f$ is given by $\delta = \sqrt{2/(\sigma\omega\mu_0)}$, where σ is the conductivity of the conductors and $\mu_0 = 4\pi 10^{-7}$ H/m their permeability. The normalized or *reduced frequency* X is defined as follows:

$$X = \frac{r}{\delta} = \sqrt{f} \cdot r \sqrt{\pi\sigma\mu_0}. \quad (3)$$

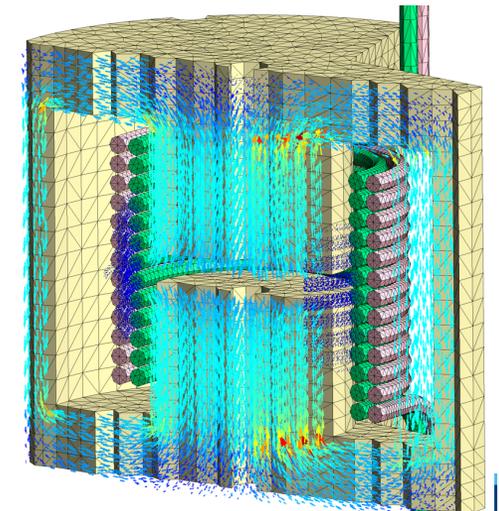
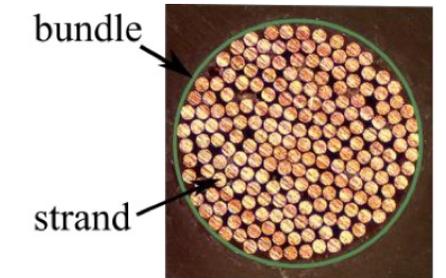
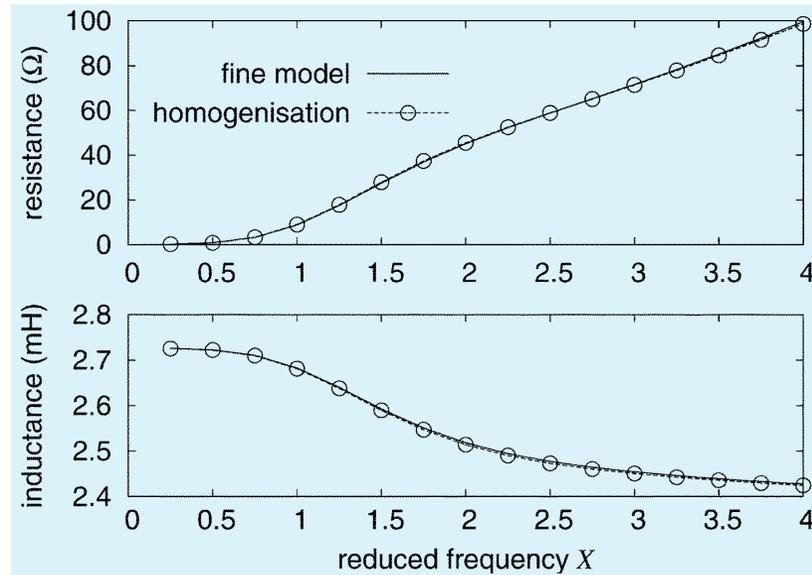
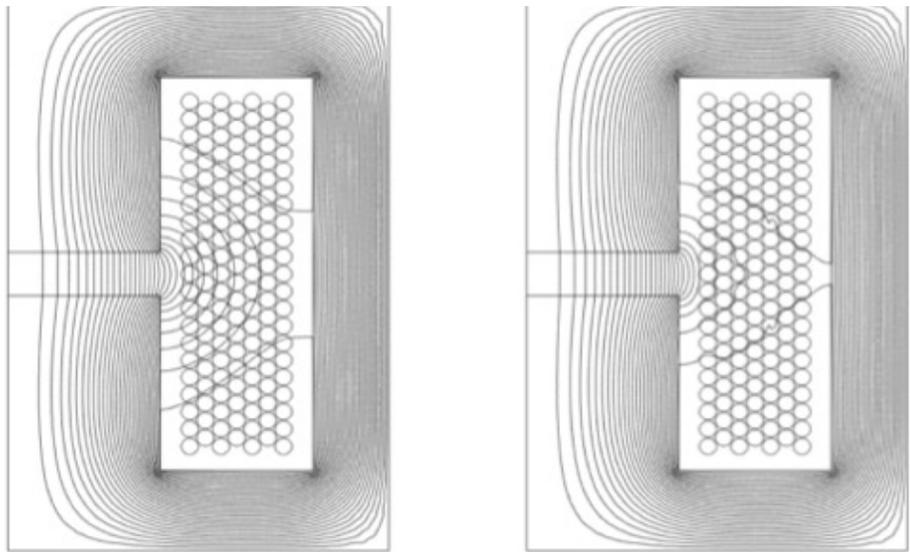
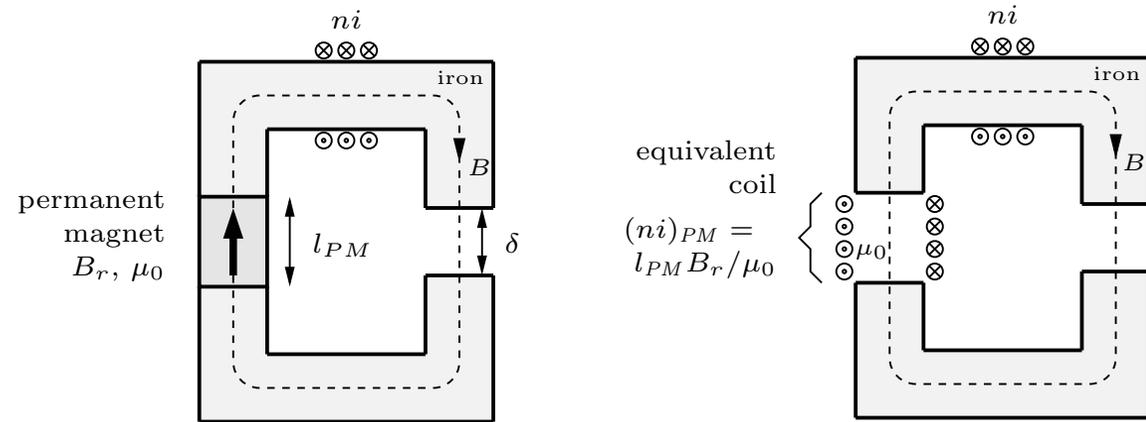
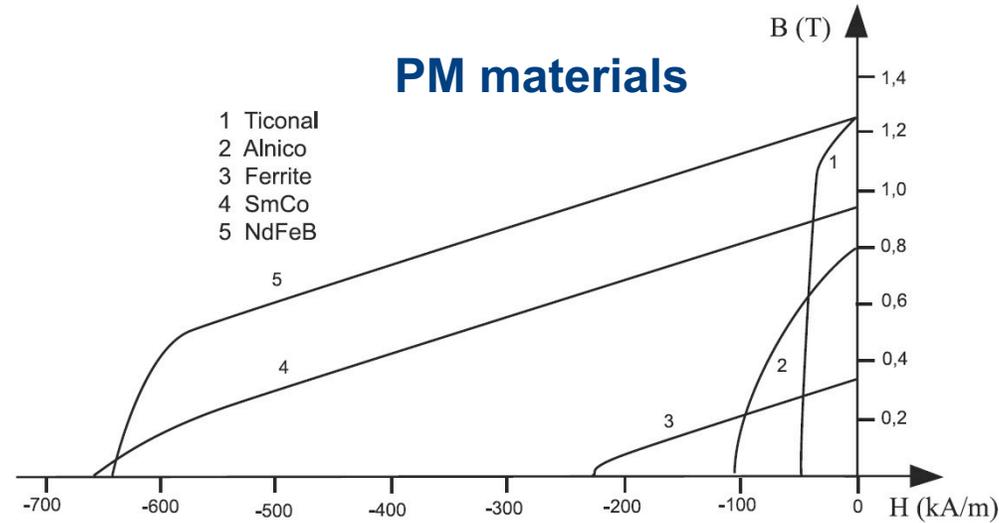


Fig. 5: 2D axisymmetric model of inductor (round conductors and hexagonal packing) – flux lines (real part, i.e. in phase with imposed current), at $X = 0.1$ (left) and $X = 2$ (right), obtained with fine model

Permanent magnet Scalar & linear model



Very simple magnetic model

✓ resulting flux approximately aligned

✓ operation point in linear range

MVP formulation

$$\text{curl}(\nu \text{curl} \mathbf{a}) = \mathbf{j} - \underbrace{\text{curl} \mathbf{h}_m}_{\text{magnetization current}}$$

2D

magnetization current

$$-\partial_x(\nu \partial_x a_z) - \partial_y(\nu \partial_y a_z) = j_z - \partial_x h_{m,y} + \partial_y h_{m,x}$$

$$b = b_r + \mu h$$

$$h = h_m + \nu b$$

