

Electromagnetic Energy Conversion - ELEC0431 : Introduction to exercise sessions

5 February 2021

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Exercise sessions are organized on Friday mornings from 10.30 am to 12.30 am.

The exercise manual will be updated for each theme of the course.

Themes

- Useful reminders
- Transformers
- AC synchronous machines
- AC asynchronous machines
- DC machines
- Electronic control systems

4 sessions

- Laboratory session 1: Transformers,
- Laboratory session 2: AC synchronous machines,
- Laboratory session 3: AC asynchronous machines.
- Laboratory session 4: DC machines,

The lab sessions will be provided through podcasts. At the end of the semester, face-to-face sessions might be organized if the sanitary conditions permit it.

The manual of laboratory will be updated concurrently with the podcasts.

The logo consists of a blue square with a vertical gradient from light blue at the top to a darker blue at the bottom. The word "wooclap" is written in white, lowercase, sans-serif font in the center of the square.

wooclap

Course Introduction

Wooclap code : HKEOZH

ELEC0431 : Exercise session 1

Reminders of phasors and power in the sinusoidal steady state

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The logo for Wooclap, consisting of a blue square with the word "wooclap" in white lowercase letters.

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Phasors and complex power

Wooclap code : OSKIYB

The phasor definition

$$\begin{aligned} f(t) &= \underbrace{\sqrt{2} F_{\text{RMS}}}_{\text{amplitude}} \cos \left(\underbrace{\omega}_{\text{pulsation}} t + \underbrace{\theta}_{\text{phase angle}} \right) \\ &= \text{Re} \left(\sqrt{2} F_{\text{RMS}} e^{j(\omega t + \theta)} \right) \\ &= \text{Re} \left(\sqrt{2} \underbrace{F_{\text{RMS}} e^{\theta}}_{\bar{F}} e^{j\omega t} \right) \end{aligned}$$

\bar{F} , the phasor of $f(t)$ is a complex number, with its amplitude and its phase angle.

The phasor definition

The main assumptions of the phasor approximation are a constant frequency and linearity.

Linearity ensured as Kirchhoffs' laws and differential equations are linear.

Time domain		Frequency domain
$f(t)$	\iff	\bar{F}
$a f(t) + b g(t)$	\iff	$a \bar{F} + b \bar{G}$
$\frac{d \cdot}{dt}$	\iff	$j \omega$
$\int \cdot dt$	\iff	$\frac{1}{j \omega}$

RMS value and peak value

The Root Mean Square (RMS) value of a function, also called the effective value is defined by

$$F_{\text{RMS}} := \sqrt{\frac{1}{T} \int_0^T f(t)^2 dt} \quad (1)$$

In the case of a harmonic function of angular frequency ω , where the base period of the function is $T = \frac{2\pi}{\omega}$,

$$F_{\text{peak}} = \sqrt{2} F_{\text{RMS}} \quad (2)$$

which is the result of the following calculations :

$$\begin{aligned} \int_0^T f(t)^2 dt &= \int_0^T F_{\text{peak}}^2 \cos^2(\omega t + \theta) dt \\ &= \frac{F_{\text{peak}}^2}{2} T \end{aligned}$$

Product of 2 harmonic functions

In the continuity of the phasor definition, one can present the product of two harmonic functions as

$$\begin{aligned} f(t) g(t) &= F_{\text{peak}} \cos(\omega t + \theta) \quad G_{\text{peak}} \cos(\omega t + \psi) \\ &= 2 F_{\text{RMS}} G_{\text{RMS}} \cos(\omega t + \theta) \cos(\omega t + \psi) \\ &= F_{\text{RMS}} G_{\text{RMS}} \left[\underbrace{\cos(\theta - \psi)}_{\text{DC, 0 Hz}} + \cos(2\omega t + \theta + \psi) \right] \end{aligned}$$

The simplification of the factor of 2 justifies the definition of the phasor as

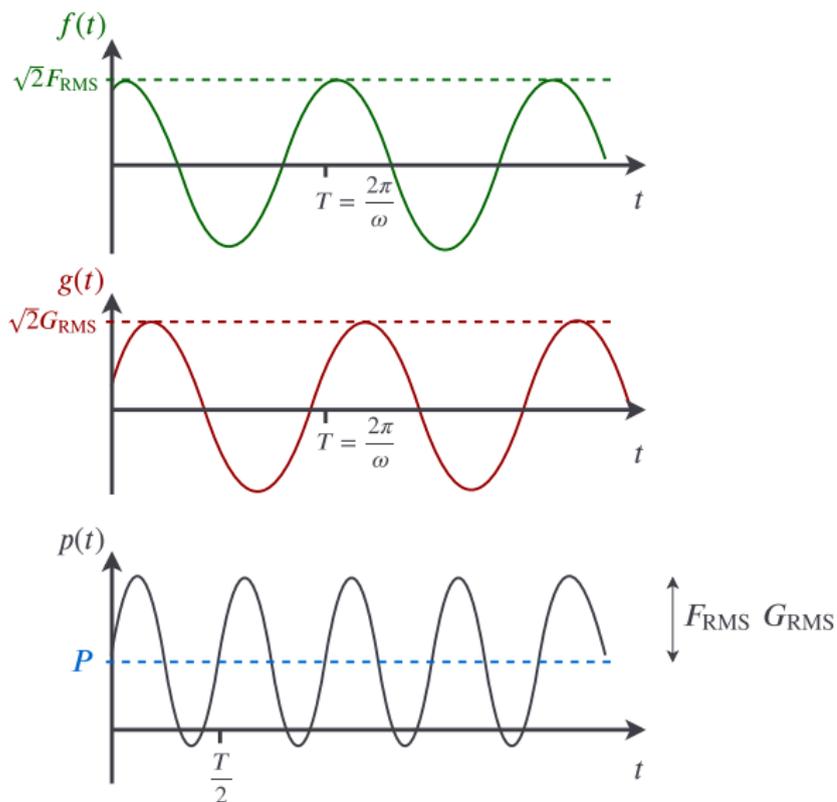
$$\boxed{\bar{F} = F_{\text{RMS}} e^{j\theta}} \quad (3)$$

The instantaneous power $p(t)$

In the time domain, the definition of the instantaneous power $p(t)$ is expressed as the product

$$\begin{aligned} p(t) &= f(t) g(t) \\ &= \underbrace{F_{\text{RMS}} G_{\text{RMS}} \cos(\theta - \psi)}_P + \underbrace{F_{\text{RMS}} G_{\text{RMS}} \cos(2\omega t + \theta + \psi)}_{p_f(t)} \end{aligned}$$

The instantaneous power $p(t)$



The instantaneous power $p(t)$

The instantaneous power can be further developed

$$\begin{aligned} p(t) &= F_{\text{RMS}} G_{\text{RMS}} (\cos(\theta - \psi) + \cos(2\omega t + \theta + \psi)) \\ &= F_{\text{RMS}} G_{\text{RMS}} (\cos(\theta - \psi) + \cos(2(\omega t + \theta) - (\theta - \psi))) \\ &= F_{\text{RMS}} G_{\text{RMS}} (\cos(\theta - \psi) + \cos(2(\omega t + \theta)) \cos(\theta - \psi) \\ &\quad + \sin(2(\omega t + \theta)) \sin(\theta - \psi)) \\ &= \underbrace{F_{\text{RMS}} G_{\text{RMS}} \cos(\theta - \psi)}_{P, \text{ the active power}} (1 + \cos(2(\omega t + \theta))) \\ &\quad + \underbrace{F_{\text{RMS}} G_{\text{RMS}} \sin(\theta - \psi)}_{Q, \text{ the reactive power}} \sin(2(\omega t + \theta)) \end{aligned}$$

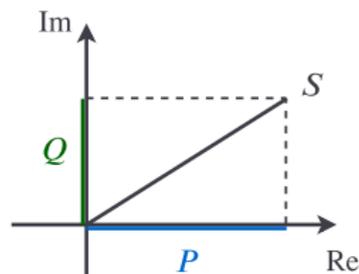
The complex power S

The power, here defined as the product of two harmonic functions, can be expressed in the frequency domain (*i.e.* with phasors). It is then called the complex power

$$S = \overline{F} \overline{G}^* \quad (4)$$

$$\begin{aligned} &= F_{\text{RMS}} G_{\text{RMS}} \cos(\theta - \psi) + j F_{\text{RMS}} G_{\text{RMS}} \sin(\theta - \psi) \\ &= \quad \quad \quad P \quad \quad \quad + j \quad \quad \quad Q \quad \quad \quad \quad (5) \end{aligned}$$

where one can retrieve the active power P and the reactive power Q as previously defined.



Important note about the notations

Remark : The following conventions will be used in the rest of the course for RMS and peak value.

$$F_{\text{RMS}} \quad \Longrightarrow \quad F \quad (V \text{ and } I)$$

$$F_{\text{peak}} \quad \Longrightarrow \quad F_m \quad (V_m \text{ and } I_m)$$

The concept of phasor can be applied to electrical quantities such as voltages and currents

Time domain

$$v(t) = \sqrt{2} V \cos(\omega t + \theta)$$

$$i(t) = \sqrt{2} I \cos(\omega t + \psi)$$

\iff

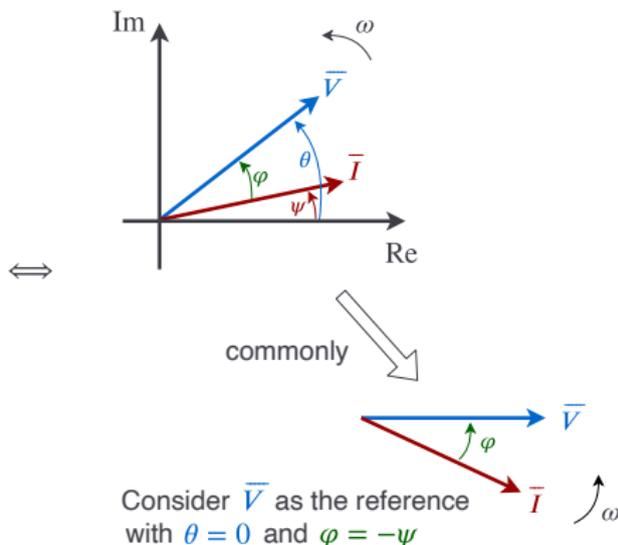
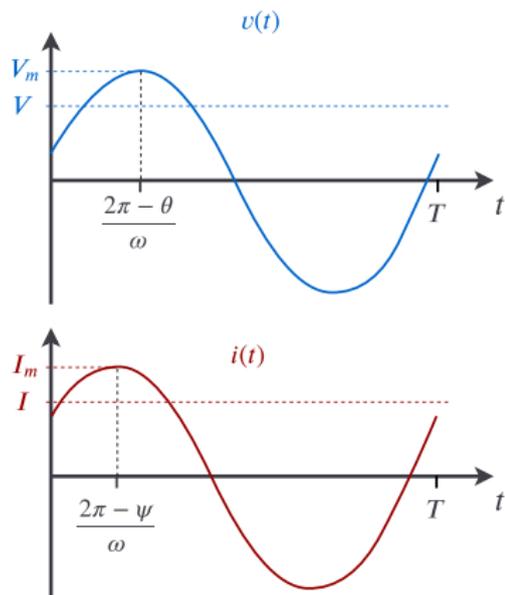
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Frequency domain

$$\bar{V} = V e^{j\theta}$$

$$\bar{I} = I e^{j\psi}$$

Alternating voltages and currents - Phasor diagrams



$$\phi = \theta - \psi$$

(6)

The complex power (for electrical quantities) and the apparent power

The definition of the complex power remains exactly the same for electrical quantities

$$\begin{aligned} S &= \overline{V} \overline{I}^* & (7) \\ &= V e^{j\theta} I e^{j(-\psi)} \\ &= V I e^{j(\theta-\psi)} \\ &= V I e^{j\varphi} \\ &= V I \cos(\varphi) + j V I \sin(\varphi) \\ &= P + j Q \end{aligned}$$

Based on that definition, one also defines the apparent power as the norm of the complex power :

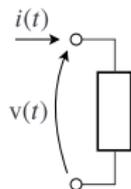
$$|S| = \sqrt{P^2 + Q^2} = V I \quad (8)$$

Power reference of the one-port ("le dipôle")

The signal $v(t)$ is the voltage across the one-port.

The signal $i(t)$ is the current through the one-port.

The "motor" convention



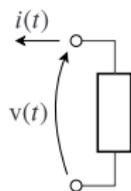
$$i(t) > 0$$

$$p(t) = v(t) i(t)$$

when it enters by the top of the one-port.

is the instantaneous power absorbed by the one-port.

The "generator" convention



$$i(t) > 0$$

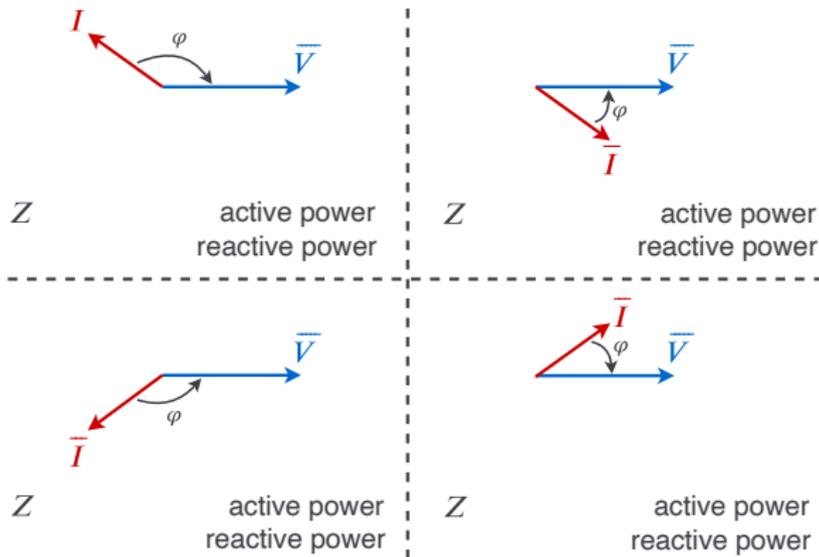
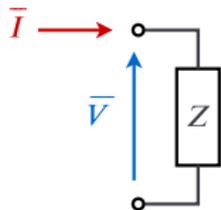
$$p(t) = v(t) i(t)$$

when it leaves by the top of the one-port.

is the instantaneous power produced by the one-port.

Consumer or producer ?

"Motor" convention :

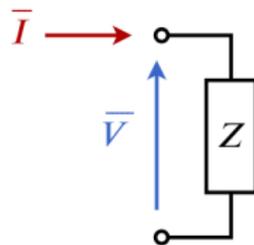


When $|\varphi| < \frac{\pi}{2}$: The load active power ($\cos(\varphi) > 0$)

When $\underbrace{\varphi > 0}_{(\bar{I} \text{ is lagging } \bar{V})}$: The load reactive power ($\sin(\varphi) > 0$)

Consumer or producer ?

"Motor" convention :



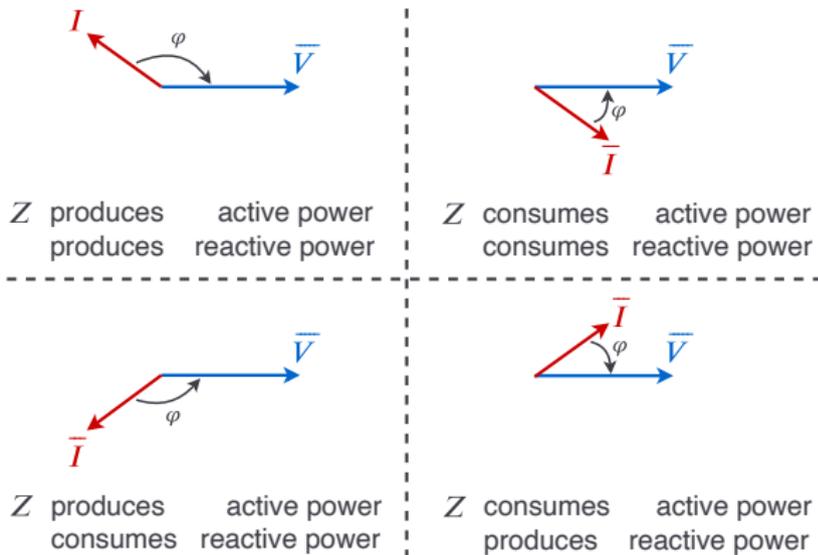
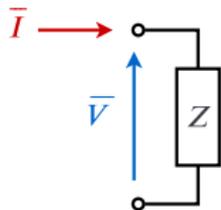
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Consumer or Producer

Wooclap code : OXYARO

Consumer or producer - solution

"Motor" convention :



When $|\varphi| < \frac{\pi}{2}$: The load consumes active power ($\cos(\varphi) > 0$)

When $\underbrace{\varphi > 0}_{(\bar{I} \text{ is lagging } \bar{V})}$: The load consumes reactive power ($\sin(\varphi) > 0$)

Expressions relative to one-ports

$$\bar{V} = Z \bar{I} = (R + j X) \bar{I}$$

$$\bar{I} = Y \bar{V} = (G + j B) \bar{V}$$

Z : the impedance $[\Omega]$

R : the resistance $[\Omega]$

X : the reactance $[\Omega]$

Y : the admittance $[S]$

G : the conductance $[S]$

B : the susceptance $[S]$

$$S = Z I^2 \quad [VA]$$

$$P = R I^2 \quad [W]$$

$$Q = X I^2 \quad [var]$$

$$S = Y^* V^2 \quad [VA]$$

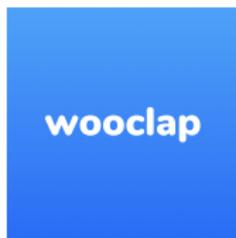
$$P = G V^2 \quad [W]$$

$$Q = -B V^2 \quad [var]$$

Power consumption of basic one-ports

	R	L	C
φ	0	$\frac{\pi}{2}$	$-\frac{\pi}{2}$
P	$R I^2 = \frac{V^2}{R}$	0	0
Q	0	$X I^2 = \omega L I^2 = \frac{V^2}{\omega L}$	$-B V^2 = -\omega C I^2 = -\frac{I^2}{\omega C}$

Exercises



Exercises of session 1

Wooclap code : QBSBER

Exercise 1 : voltage distribution

The circuit of Figure 1 presents a resistive-inductive load powered with an AC generator of sinusoidal voltage (230 V, 50 Hz). Find the voltages across R and L (magnitude and phase angle) and represent all the voltages on a phasor diagram.

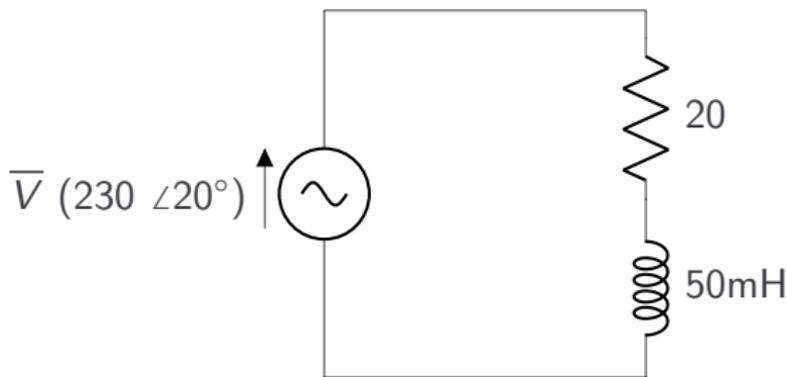
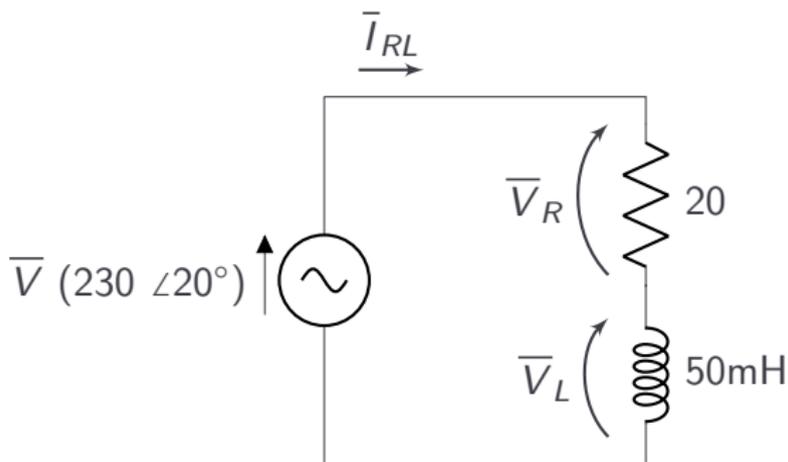


Figure: Resistive-inductive circuit.

Exercise 1 : voltage distribution - solution



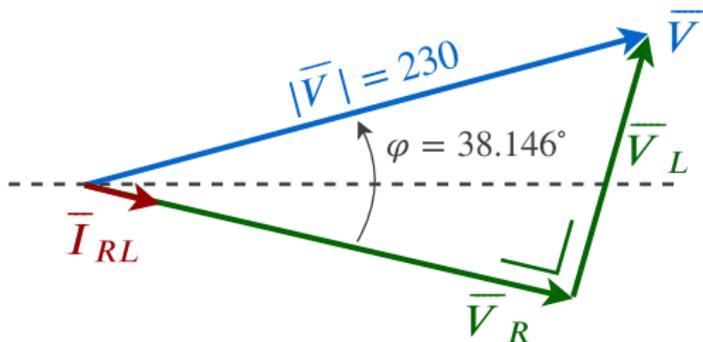
$$\bar{V} = \underbrace{R \bar{I}_{RL}}_{\bar{V}_R} + \underbrace{j X_L \bar{I}_{RL}}_{\bar{V}_L} = (R + j X_L) \bar{I}_{RL} \quad (9)$$

$$\bar{I}_{RL} = \frac{\bar{V}}{(R + j X_L)} = \frac{230 \angle 20^\circ}{20 + j 15.708} = 9.044 \angle -18.146^\circ \quad (10)$$

Exercise 1 : voltage distribution - solution

$$\bar{V}_R = R \bar{I}_{RL} = 180.881 \angle -18.146^\circ \quad [\text{V}] \quad (11)$$

$$\bar{V}_L = j X_L \bar{I}_{RL} = 142.064 \angle 71.854^\circ \quad [\text{V}] \quad (12)$$



The reactive power consumed by the load is

$$Q = V I_{RL} \sin(\varphi) = 230 \times 9.044 \times \sin(38.146^\circ) = 1284.82 \quad [\text{var}] \quad (13)$$

Exercise 2 : reactive power compensation

Your colleague suggests to add a $50\ \mu\text{F}$ capacitor in parallel of the RL load. It is supposed to compensate the reactive power consumed by the inductive load. Is it a good idea ? If so, what would be the exact value of C needed ?

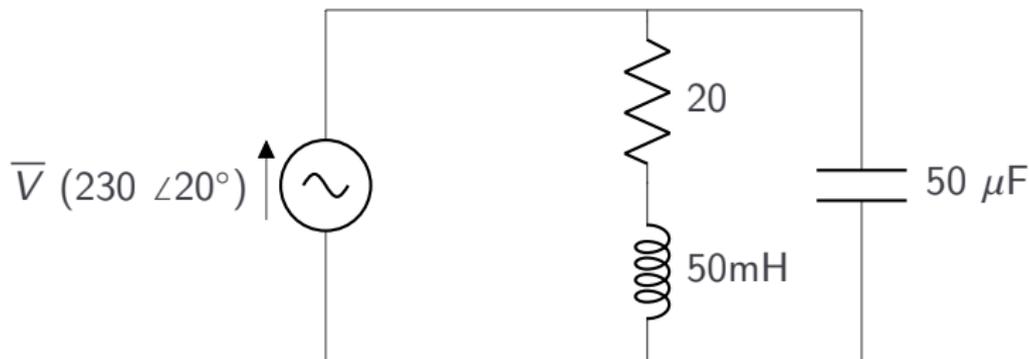
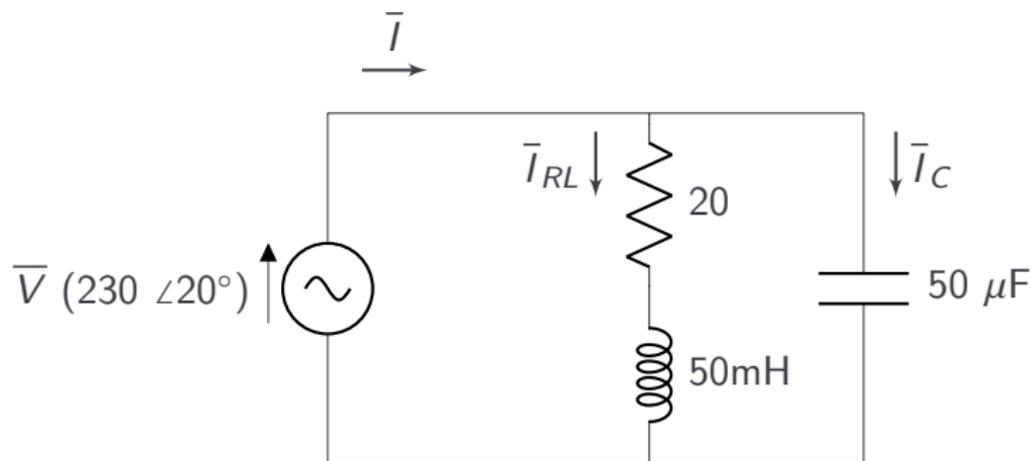


Figure: Inductive circuit with compensation capacitor.

Exercise 2 : reactive power compensation - solution



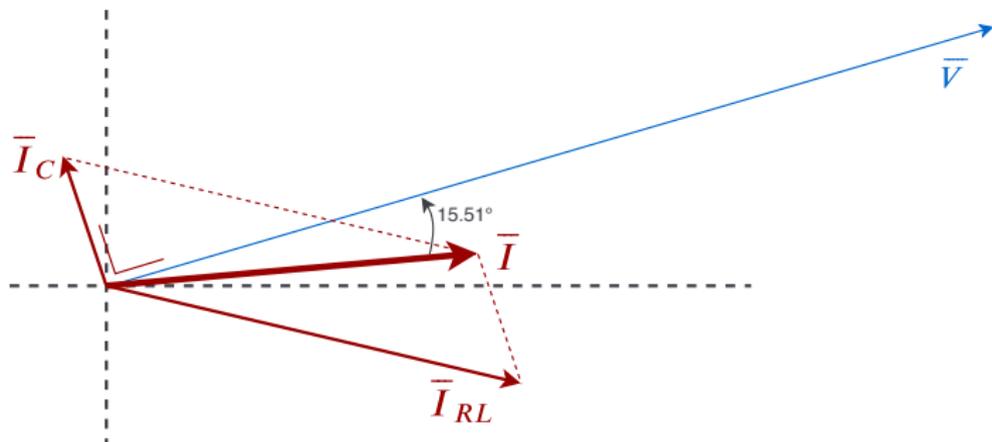
The voltage across the RL load remains the same ($\bar{V} = 230 \angle 20^\circ$). Then, the current in RL is still $\bar{I}_{RL} = 9.044 \angle -18.146^\circ$ [A] and

$$\bar{I}_C = \frac{\bar{V}}{Z_C} = Y_C \bar{V} = j \omega C \bar{V} = 3.61 \angle 110^\circ \quad (14)$$

Exercise 2 : reactive power compensation - solution

Apply the KCL (Kirchhoff Circuit Law) and obtain

$$\bar{I} = \bar{I}_{RL} + \bar{I}_C = 7.381 \angle 4.49^\circ \quad (15)$$



The reactive power consumed by the load is

$$Q = V I \sin(\varphi) = 230 \times 7.381 \times \sin(15.51^\circ) = 453.957 \text{ [var]} \quad (16)$$

Exercise 2 : reactive power compensation - solution

The exact value of capacitance to be used must cancel the reactive power consumption of the inductance, such that the reactive power produced by C matches the reactive power consumed by L,

$$Q_C = -Q_{RL} \quad (17)$$

$$-B_C V^2 = B_{RL} V^2 \quad (18)$$

$$-\omega C V^2 = -\frac{X}{R^2 + X^2} V^2 \quad (19)$$

with $B_C = \omega C$ and $B_{RL} = -\frac{\omega L}{R^2 + (\omega L)^2}$ because

$$Y_{RL} = \frac{1}{Z_{RL}} = \frac{1}{R + jX} = \frac{R - jX}{R^2 + X^2} \quad (20)$$

Thus,

$$C = \frac{L}{R^2 + (\omega L)^2} = 77.31 [\mu\text{F}] \quad (21)$$

Exercise 3 : one-port small quiz

Fill the cells of the table below with the most appropriate answer among :

=0

<0

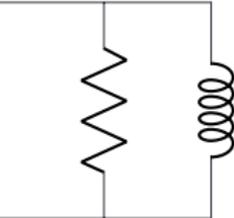
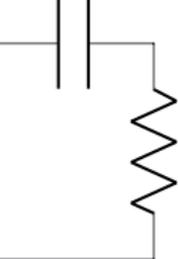
>0

=1

<1

+∞

-∞

one-port:					
active power consumed					
reactive power produced					
$\cos \phi$					
$\tan \phi$					

Exercise 3 : one-port small quiz - solution